

The Center for Astrophysical Thermonuclear Flashes

Validation of the FLASH Code: Two- and Three-Dimensional Simulations of Shock-Cylinder Interactions

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Compressible Turbulent Mixing

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An Advanced Simulation & Computing (ASC)
Academic Strategic Alliances Program (ASAP) Center
at The University of Chicago





Acknowledgements

- ❑ LANL: Chris Tomkins, Mark Marr-Lyon, Bob Benjamin
- ❑ ANL: Mike Papka, Randy Hudson
Brad Gallagher
- ❑ Vikram Dwarkadas, Tomek Plewa, Todd Dupont

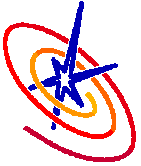
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What is the FLASH Code?

- ❑ Community code for Astrophysics - Can solve a broad range of (astro)physics problems
- ❑ Designed for compressible reactive flows
- ❑ Block-structured, spatial adaptive mesh refinement (PARAMESH)
- ❑ Parallel (MPI), including I/O
- ❑ Has a modern CS-influenced architecture
- ❑ Portable: runs on many massively-parallel systems, linux boxes to ASCI machines
- ❑ Scales and performs well - Gordon Bell prize
- ❑ Is available on the web: <http://flash.uchicago.edu>

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Verification and Validation of FLASH

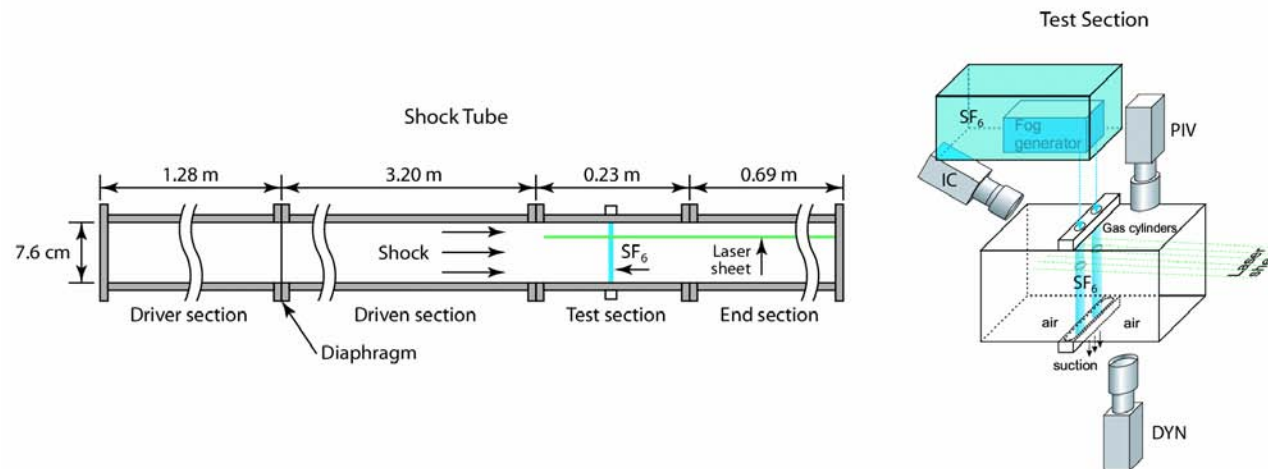
V & V at the Flash Center

- ❑ Automated test suite: standard problems run nightly on several platforms, web page to display, access results
- ❑ Verification of algorithms on problems with exact solutions; typically for components of the code base
- ❑ V&V paper: “*On Validating An Astrophysical Simulation Code*”, Calder, et al., ApJS 143, Nov. 2002. Validation for Rayleigh – Taylor and three-layer Richtmeyer-Meshkov problems.

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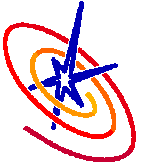


Los Alamos Shock-Cylinder Experiment



- ❑ A “cylinder” of Sulfur Hexafluoride (SF_6) falls through the air-filled test section; $M_{\text{SF}_6} \sim 5 M_{\text{air}}$
- ❑ A Mach 1.2 shock traverses the cylinder and continues down the tunnel
- ❑ Indirect SF_6 visualization, by visible-light scattering water/glycol “fog”
- ❑ Direct SF_6 visualization, by Rayleigh-scattering off SF_6 molecules
- ❑ Particle Image Velocimetry (PIV) with fog
- ❑ One image per experiment; time sequence can be constructed because of repeatability

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Flowfield Development

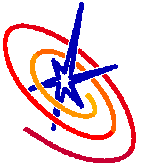
Two phases of flowfield development:

1. Shock-interaction phase:

- Misalignment of pressure and density gradients results in baroclinic vorticity deposition at the interface as the shock traverses the cylinder
- Compressible, wave dominated
- Fast, $< 50 \mu\text{s}$
- Highly sensitive to conditions before the shock arrives*

2. Instability phase:

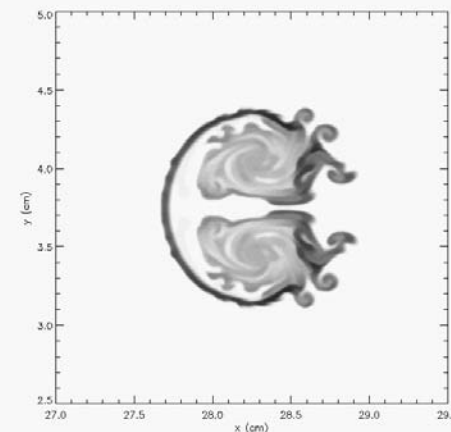
- A counter-rotating vortex pair forms, and instabilities (Kelvin-Helmholtz) develop on the interface
- Weakly compressible, dominated by viscosity, instabilities, vortex dynamics
- Slow, $\sim 800 \mu\text{s}$
- Highly sensitive to conditions established in phase 1*



Flowfield Development



- ❑ Experimental time series, water/glycol SF₆ mole fraction.
- ❑ Images correspond to 50, 190, 330, 470 ns after shock impact
- ❑ Composite image does not preserve time relationship



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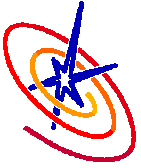
Earlier Results

Some things we looked at:

- Sensitivity to simulation parameters:
 - Resolution (numerical viscosity)
 - Adaptive Mesh Refinement (AMR)
 - Courant number
 - Mesh refinement criteria
- Velocity fields
- Double cylinder configuration
- Speculative 3D calculation

... others we could have:

- Shock strength
- Equation of state



Earlier Results

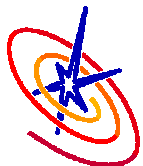
Issues/Obstacles:

Sensitivity to initial conditions:

- “Raw” RS experimental image of the initial SF₆ distribution vs. axisymmetric fit
- Initial maximum mole fraction, X_{SF_6}

There is no viscosity model. Only resolution dependent numerical viscosity is present.

Validation metric. Visual comparison of experimental and computed morphology (eyeball norm)

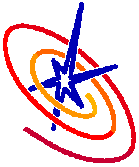


New Results

Recent work focuses on:

- Initial conditions
- Better metrics
- Three-dimensional effects

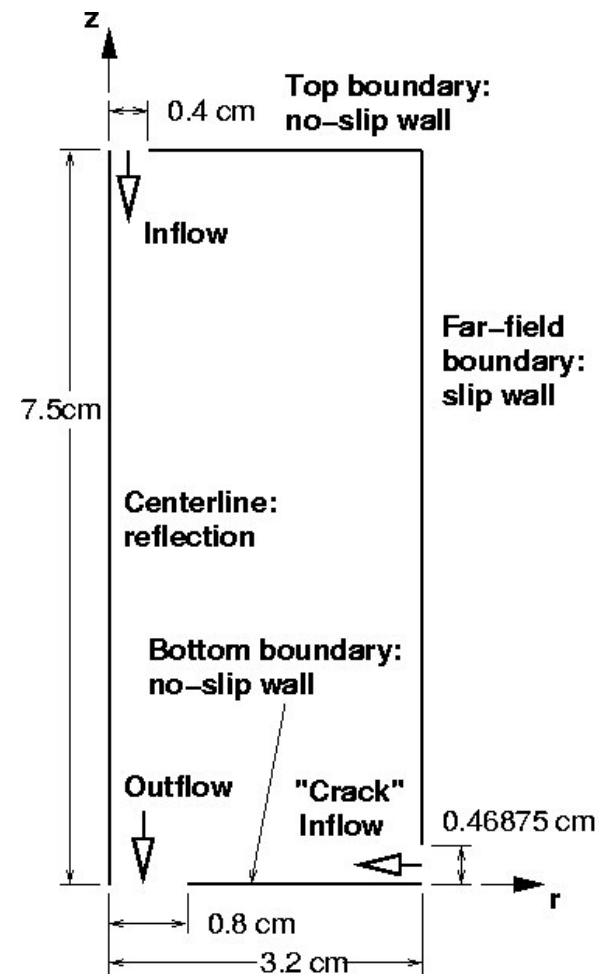
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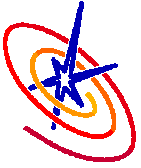
Simulations of Initial Conditions

Axisymmetric code (Todd Dupont):

- ❑ Motivation: Determine X_{SF_6}
- ❑ Motivation: Initialize three-dimensional flowfield
- ❑ Solve (single) species and momentum equations and elliptic equation for pressure
- ❑ Convection, gravity, constant viscosity, constant binary diffusion, variable density, isothermal
- ❑ Run until steady state is achieved



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Simulations of Initial Conditions

Axisymmetric code input parameters:

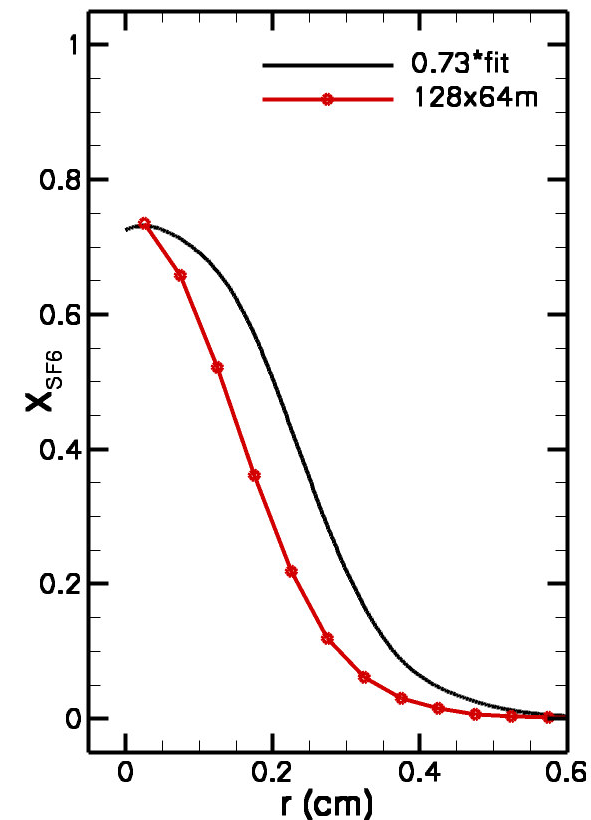
- Inlet velocity (parabolic profile)
LANL estimate: 10 cm/s
- Inlet mass fraction of SF₆
LANL estimate: 1.0
- Simulation Parameters -
Dimensions of domain, resolution,
relative sizes and flow rates

Code output:

- SF₆ mole fraction profile
Fit to experimental image
- X_{SF6} in the image plane
LANL estimate: 0.8

Inlet $Y_{\text{SF}_6} = 1.0$

Inlet $v_z = 10.0$ cm/s

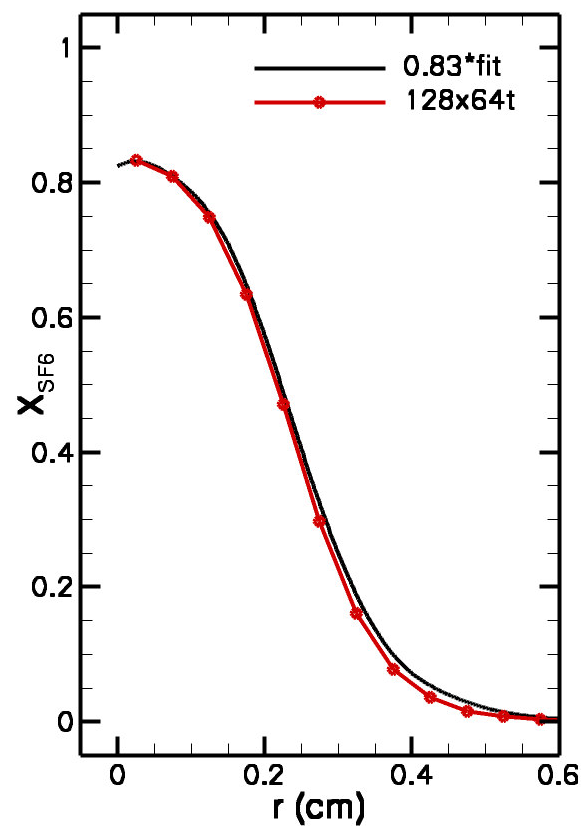
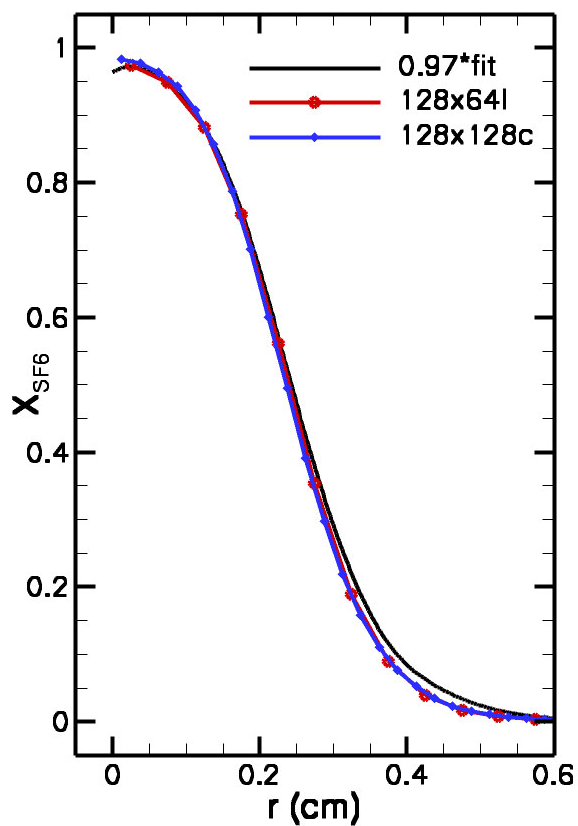




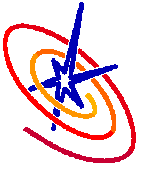
Simulations of Initial Conditions

Inlet $Y_{\text{SF}_6} = 1.0$
 Inlet $v_z = 25.0$ cm/s

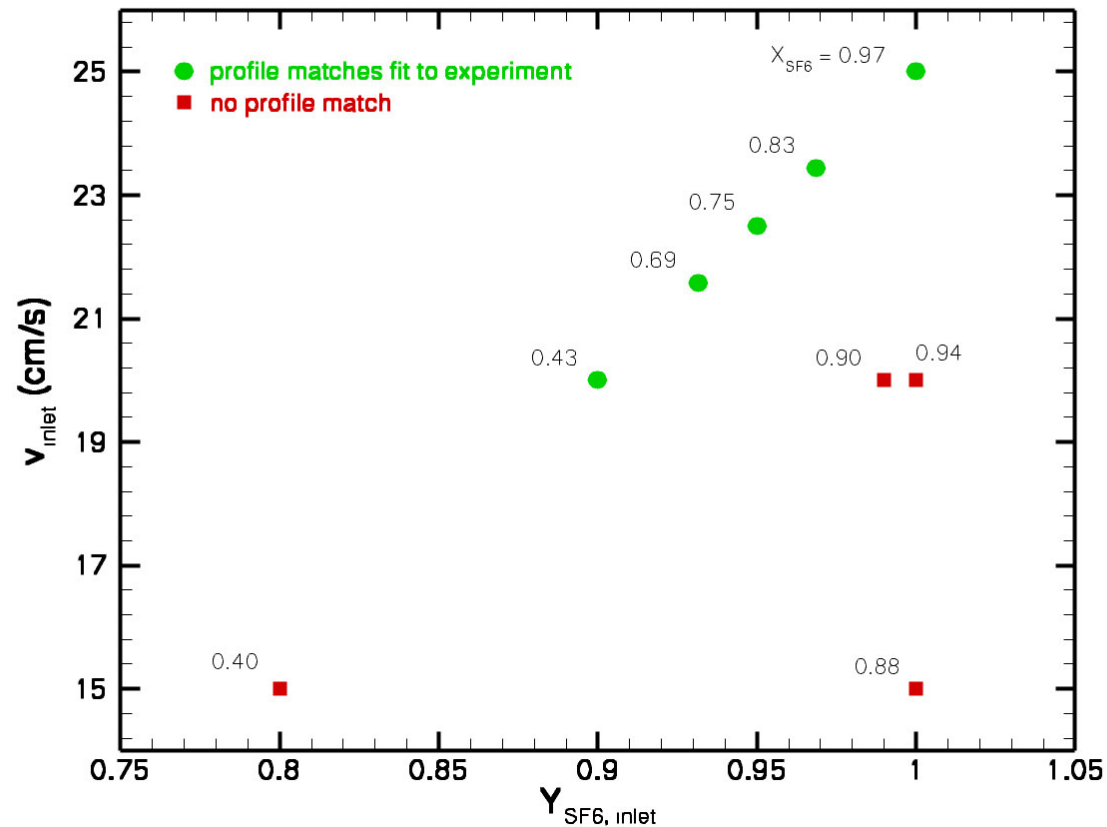
Inlet $Y_{\text{SF}_6} = 0.9685$
 Inlet $v_z = 23.43$ cm/s



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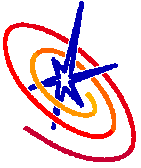


Simulations of Initial Conditions



- Initial conditions in the experimental image plane are highly sensitive to inlet conditions

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Looking for Better Metrics

While visual comparisons were ok to start with, we need a better basis for comparison to experimental data. A new metric should be:

- Quantitative
- Well-defined
- Physically meaningful

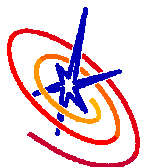
Circulation and self-induced vortex velocity both measure the vorticity deposited during the shock interaction

- Insensitive to small scale structure
- Insensitive to numerical (and physical) viscosity

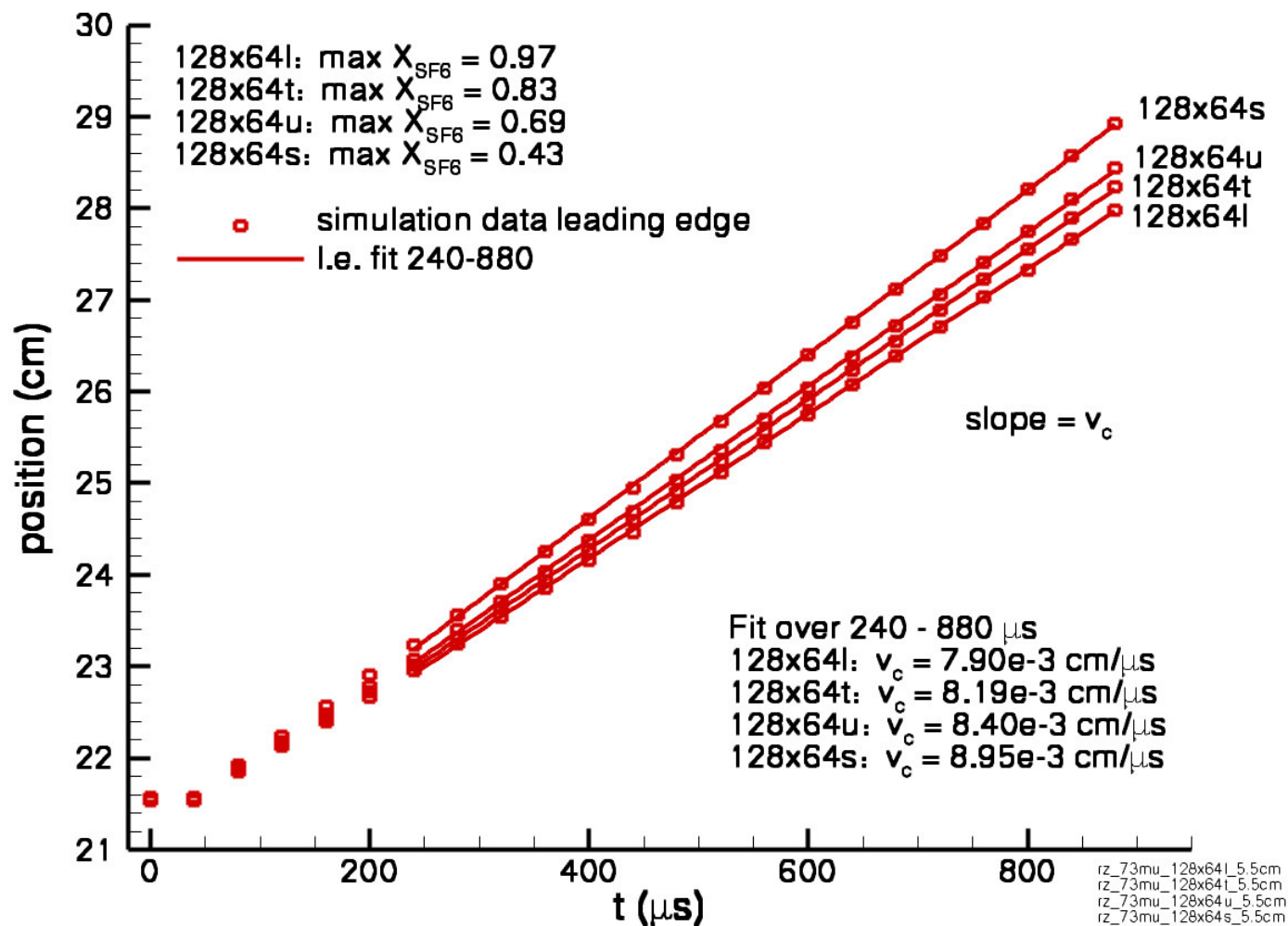
These provide:

1. A way to probe the initial composition gradients (X_{SF_6})
2. A necessary first step in correlating the vorticity deposited and the growth of secondary instabilities

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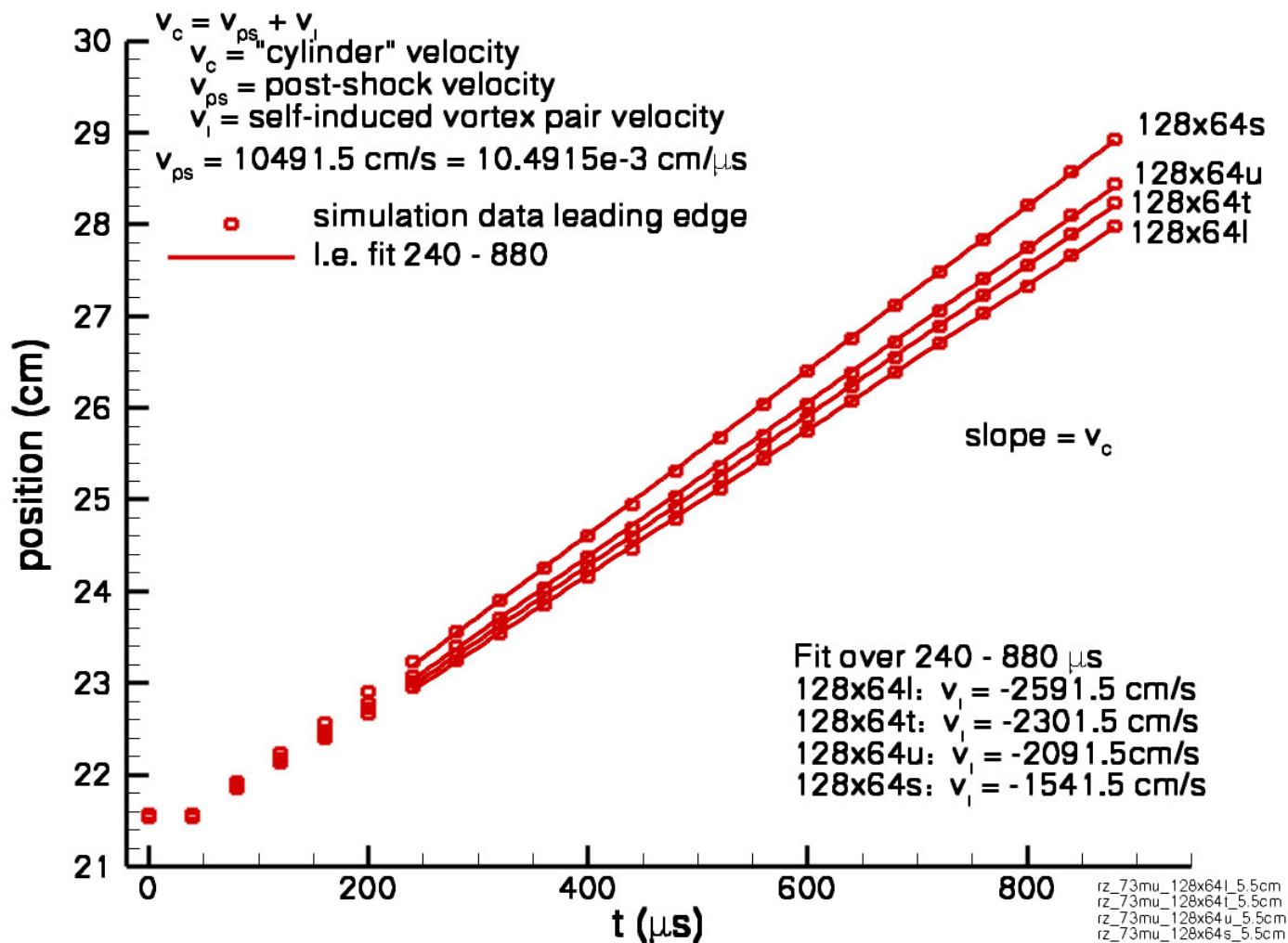
Convective Velocity



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Self-Induced Velocity



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Circulation

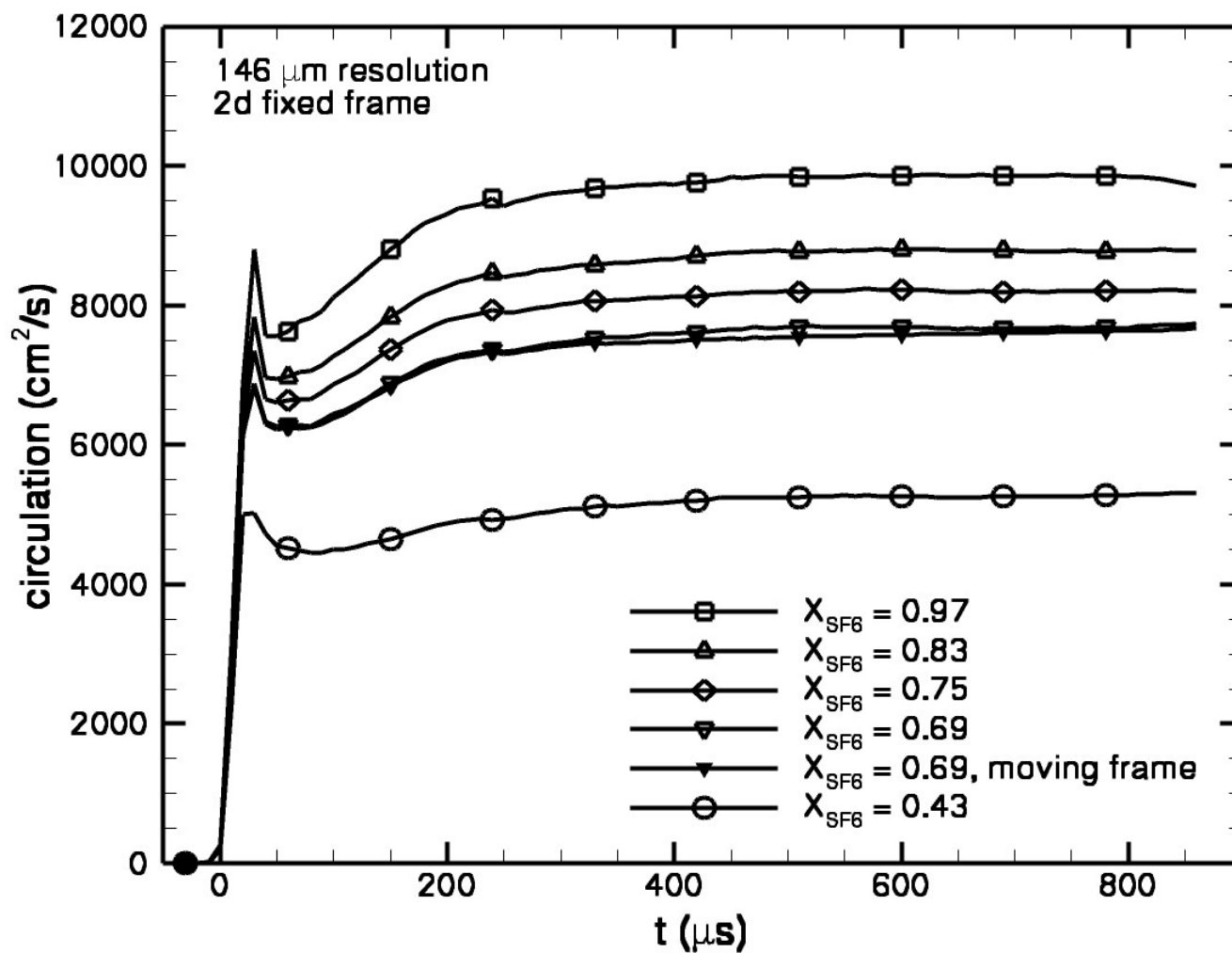
- Circulation is the integral of vorticity:

$$\Gamma = \iint \vec{\omega} \cdot d\mathbf{A}$$

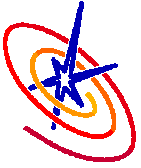
- We consider only the z-component of vorticity
- We integrate over the lower-y half of the domain (lower half in the spanwise dimension)



Circulation: Effect of Initial SF₆ Mole Fraction



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3D Simulations

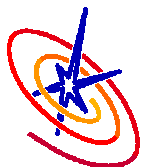
Are three-dimensional effects important?

- SF_6 and air diffuse as the SF_6 flows through the tunnel, leading to vertically varying composition, and thus density, gradients
- Instability growth and small scale structure are generally three-dimensional

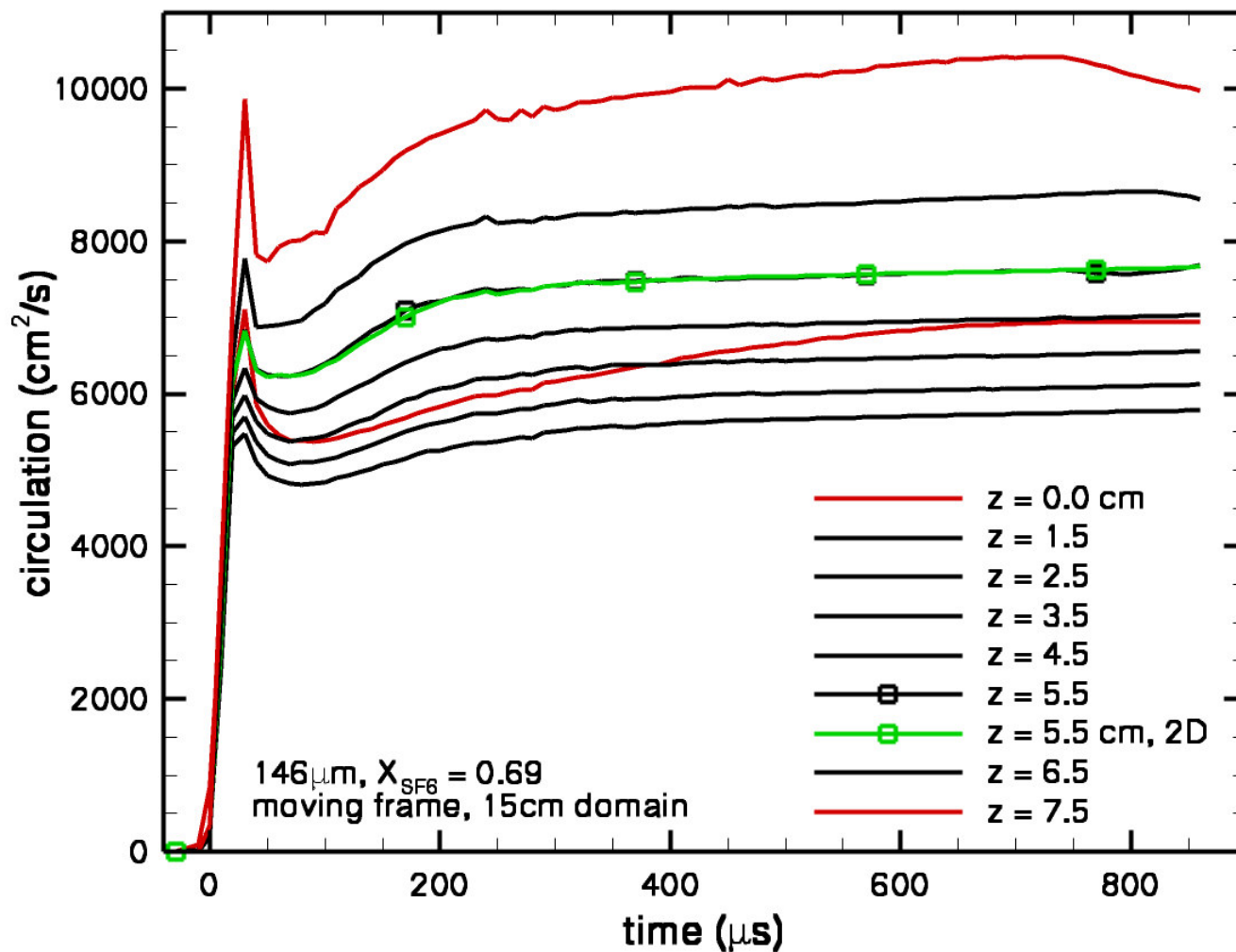
We are just beginning to analyze 3D simulations.

- Run 1: 146 μm , $X_{\text{SF}_6} = 0.97$ in image plane, fixed frame
- Run 2: 146 μm , $X_{\text{SF}_6} = 0.83$ in image plane, fixed frame
- Run 3: 146 μm , $X_{\text{SF}_6} = 0.69$ in image plane, moving frame

We have left the validation program proper – no experimental data (yet)



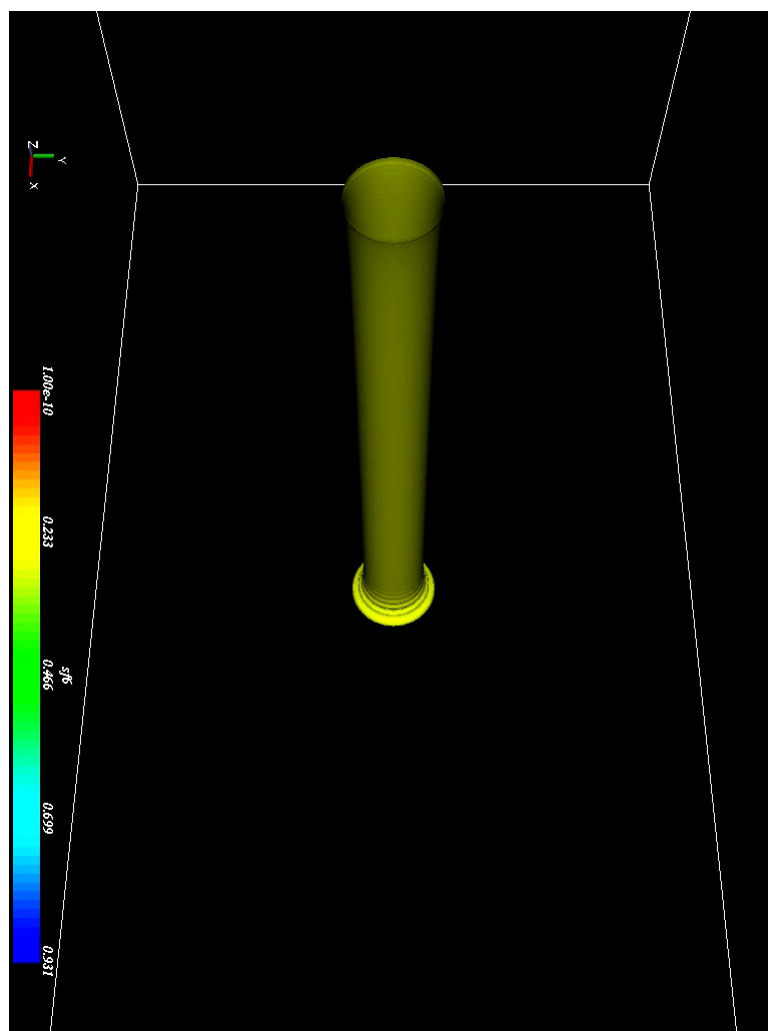
3D Simulation: Circulation



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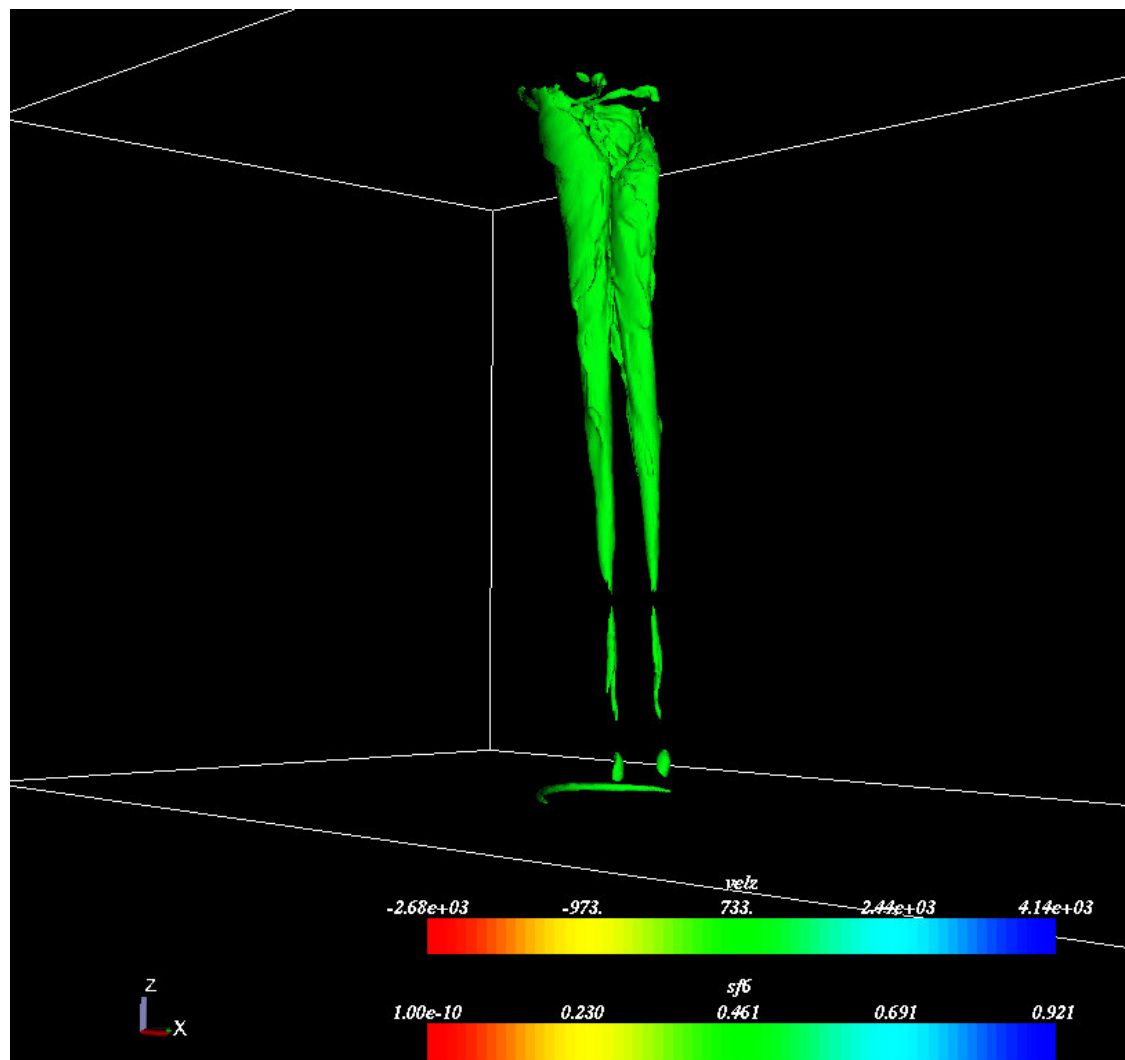
3D Simulation: Flow Visualization



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3D Simulation: Flow Visualization



$$X_{\text{SF}_6} = 0.69$$

$$t = 750 \mu\text{s}$$

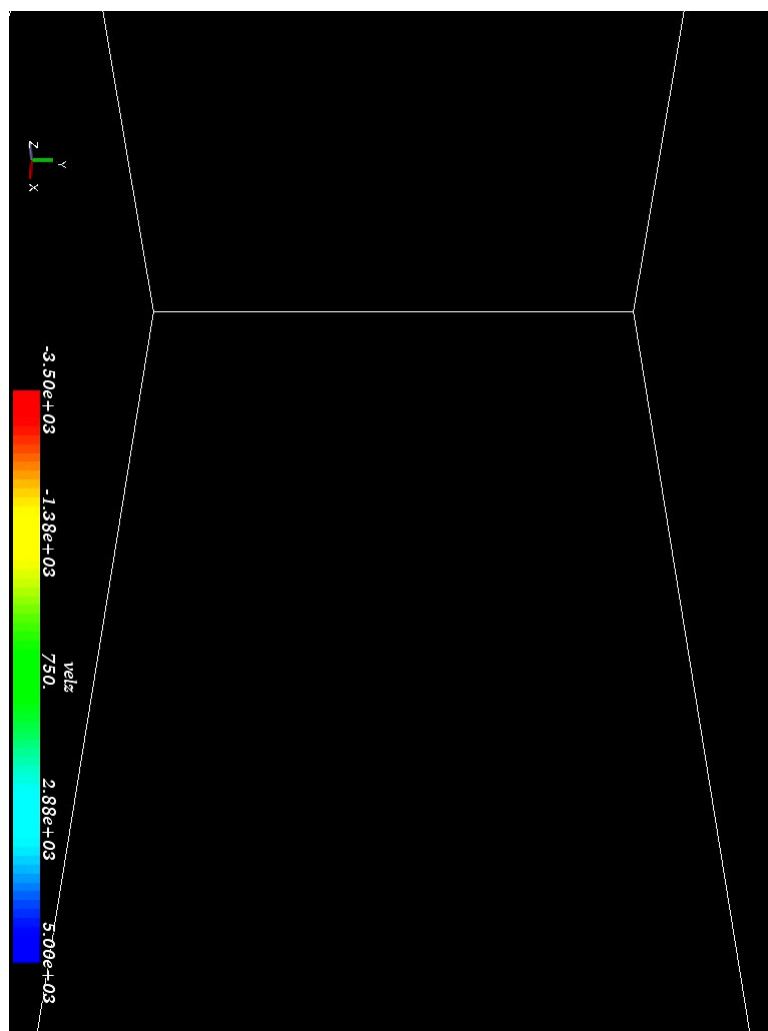
Note vertical tubes of positive z-velocity, associated with the two primary vortex cores

Spreading as the top wall is approached indicates acceleration

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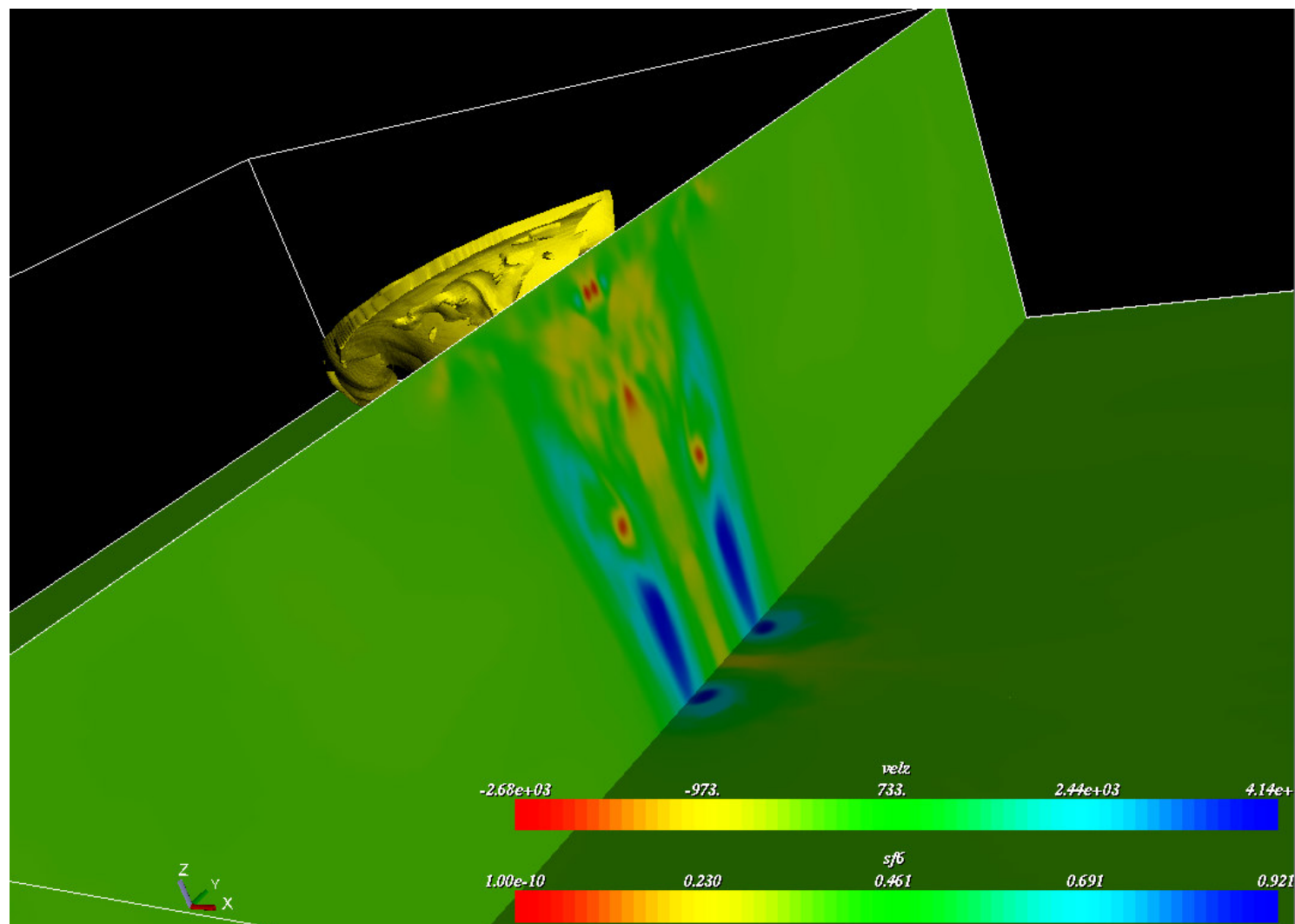
3D Simulation: Flow Visualization



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3D Simulation: Flow Visualization



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Summary

- ❑ Early validation for the shock-cylinder interaction was qualitative and focused on the influence of simulation parameters
- ❑ Work in progress:
 - ❑ Examines a range of initial conditions
 - ❑ Seeks quantitative, physically meaningful metrics
 - ❑ Examines 3D effects

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What is the FLASH Code?

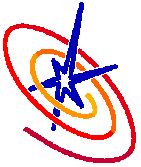
Target Applications:

- Compact accreting stars (white dwarf, neutron star)
- Reactive flows (DNS or subgrid model)
- Initial conditions close to hydrostatic equilibrium (self-gravity)
- Complex EOS (dense nuclear matter)

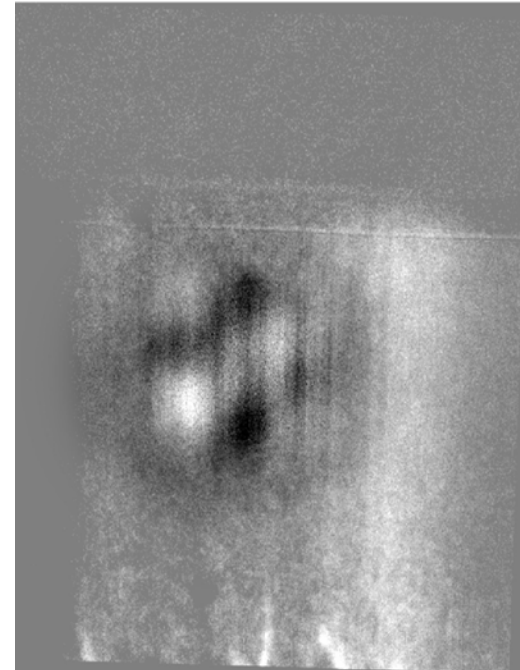
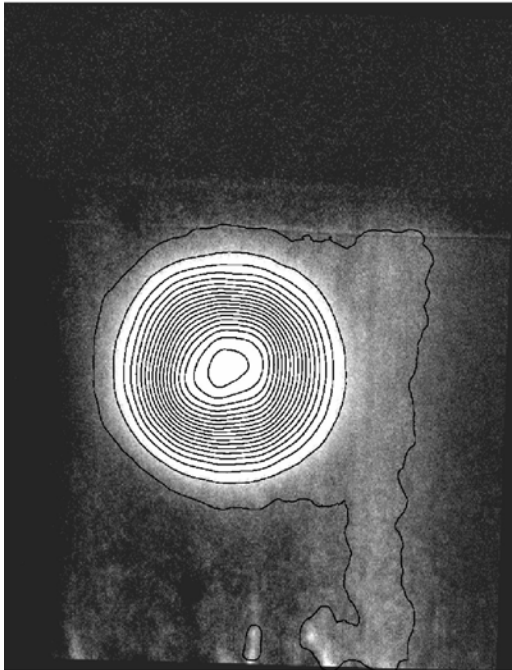
Example: Type Ia Supernova

- Massive white dwarf
- Subgrid model for nuclear flame
- Self-gravity
- Degenerate EOS

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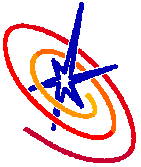


Raw Experimental Images



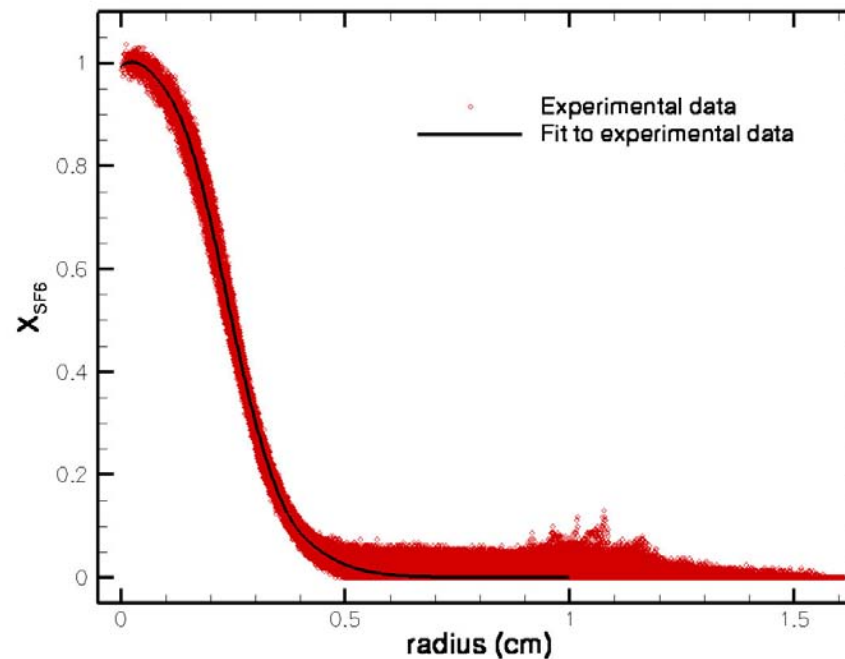
- ❑ Raw image (left) – actually, an average of several images. Pixel values are measured intensity (Rayleigh scattering,) and range from 0 to 165. (We added the contours.)
- ❑ Residual after subtracting smooth, axisymmetric fit. Pixel values range from -10 to +10.

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Axisymmetric Fit to Experimental Image

- Eventually a formula consisting of several Gaussians was developed
- Almost all of our previously published work was initialized with this fit.
- The maximum initial mole fraction of SF_6 , X_{SF_6} , must be assumed

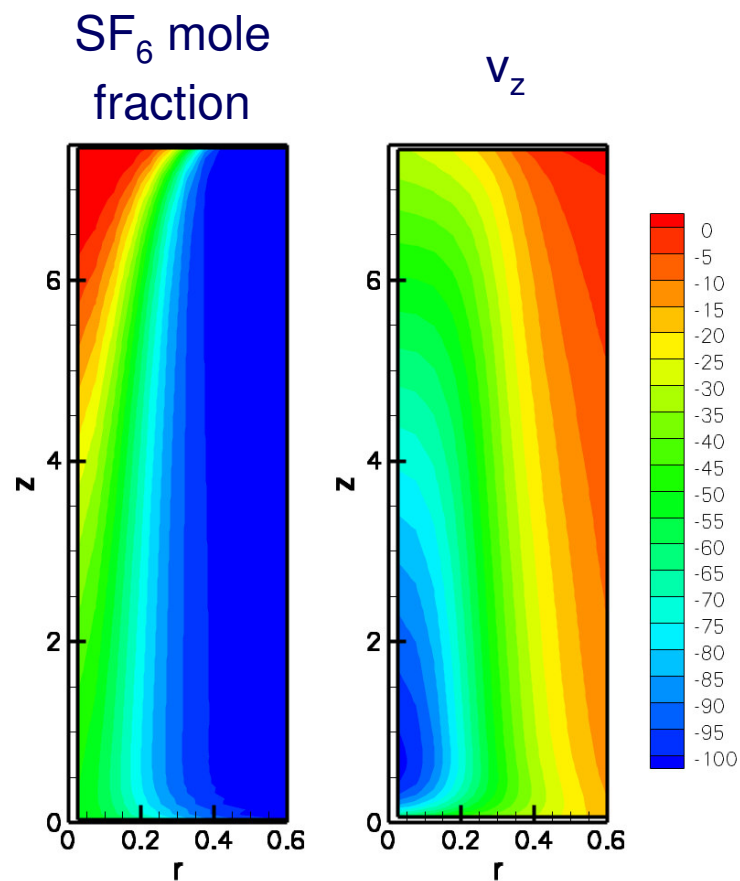


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Gravity Balances Diffusion

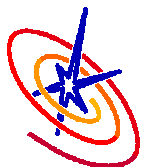
- ❑ If the inlet velocity is too low, the profile is too narrow (closer to the centerline than the experimental data): gravitational acceleration of SF₆ leads to necking
- ❑ If the velocity is too high, the profile is too steep: diffusion does not have enough time to act
- ❑ The inlet mass fraction affects the gravitational acceleration and the output X_{SF_6}



Inlet $v_z = 15.0$ cm/s

Inlet $Y_{\text{SF}_6} = 1.0$

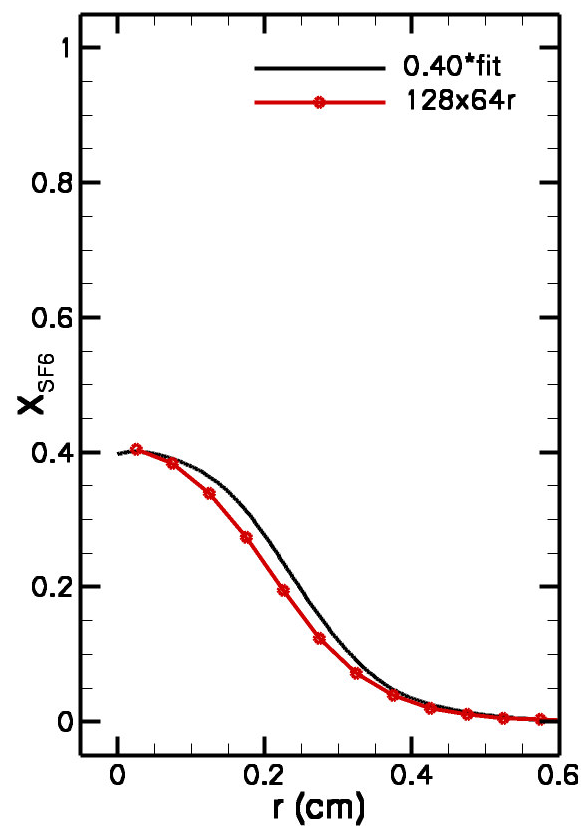
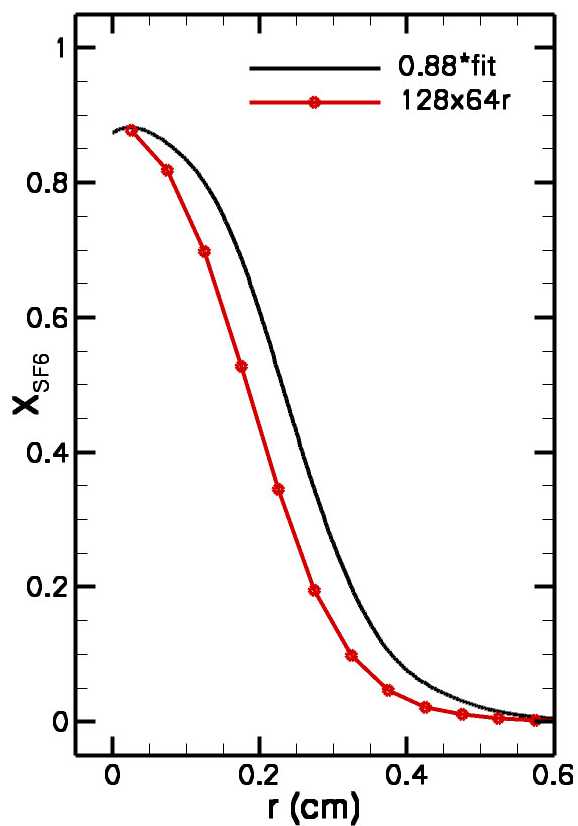
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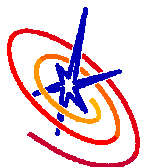
Simulations of Initial Conditions

Inlet $Y_{\text{SF}_6} = 1.0$
 Inlet $v_z = 15.0$ cm/s

Inlet $Y_{\text{SF}_6} = 0.8$
 Inlet $v_z = 15.0$ cm/s



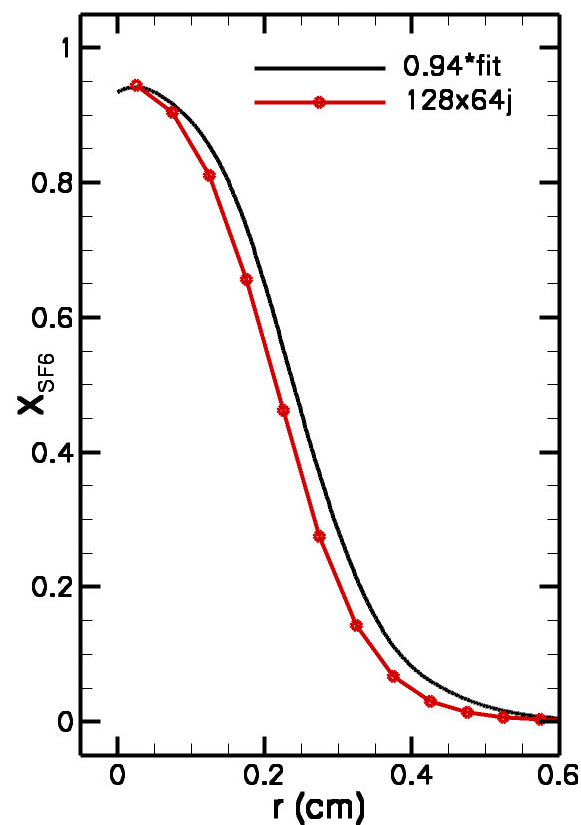
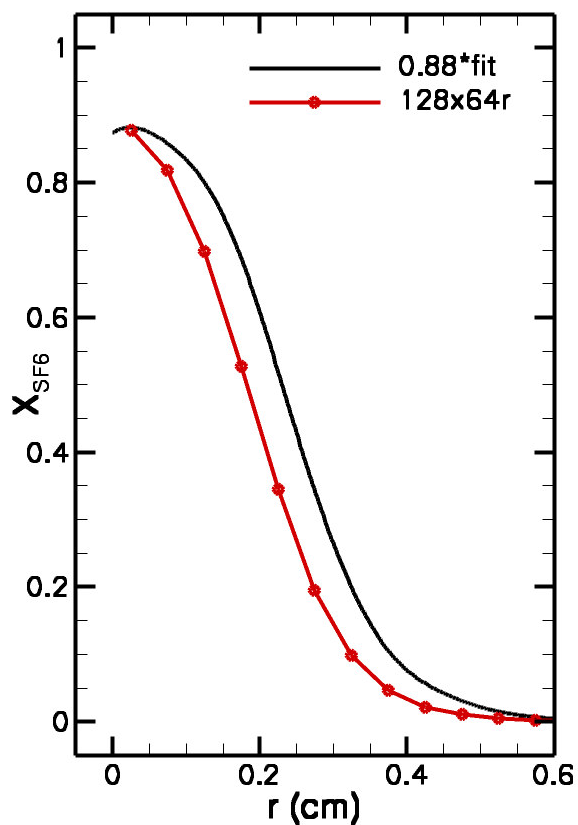
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Simulations of Initial Conditions

Inlet $Y_{\text{SF}_6} = 1.0$
 Inlet $v_z = 15.0$ cm/s

Inlet $Y_{\text{SF}_6} = 1.0$
 Inlet $v_z = 20.0$ cm/s



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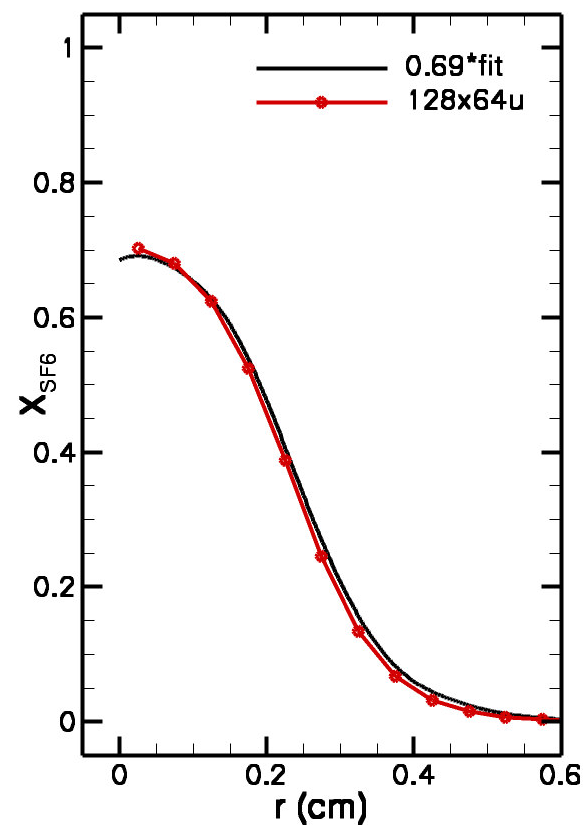
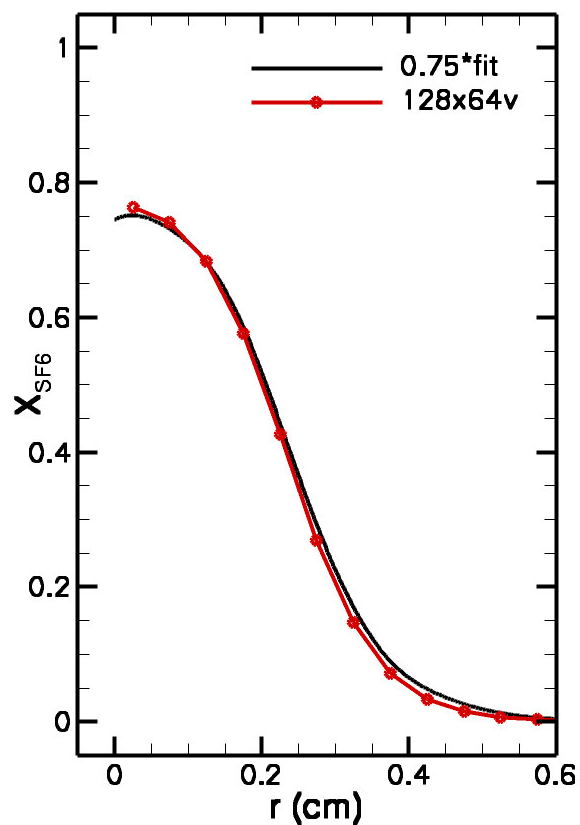
Simulations of Initial Conditions

Inlet $Y_{\text{SF}_6} = 0.95$

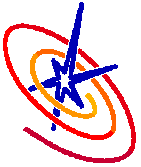
Inlet $v_z = 22.50$ cm/s

Inlet $Y_{\text{SF}_6} = 0.9315$

Inlet $v_z = 21.85$ cm/s



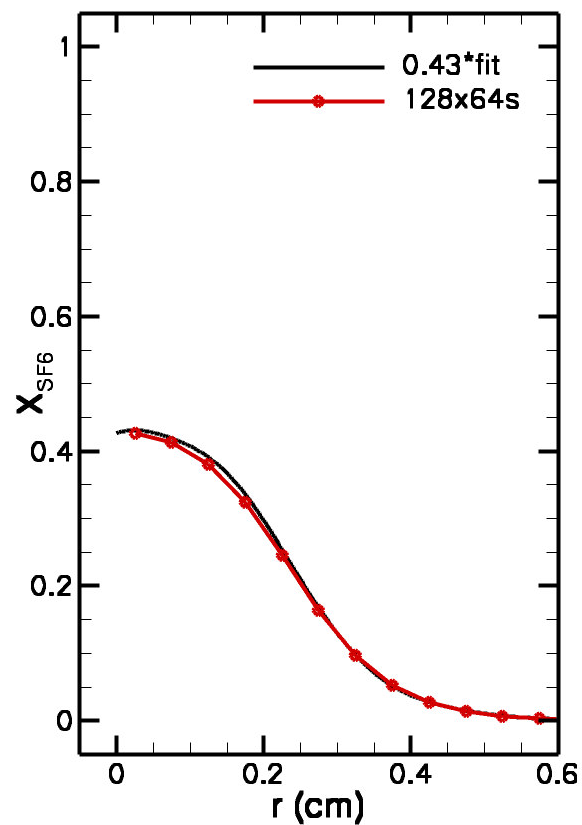
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Simulations of Initial Conditions

Inlet $Y_{\text{SF}_6} = 0.9$

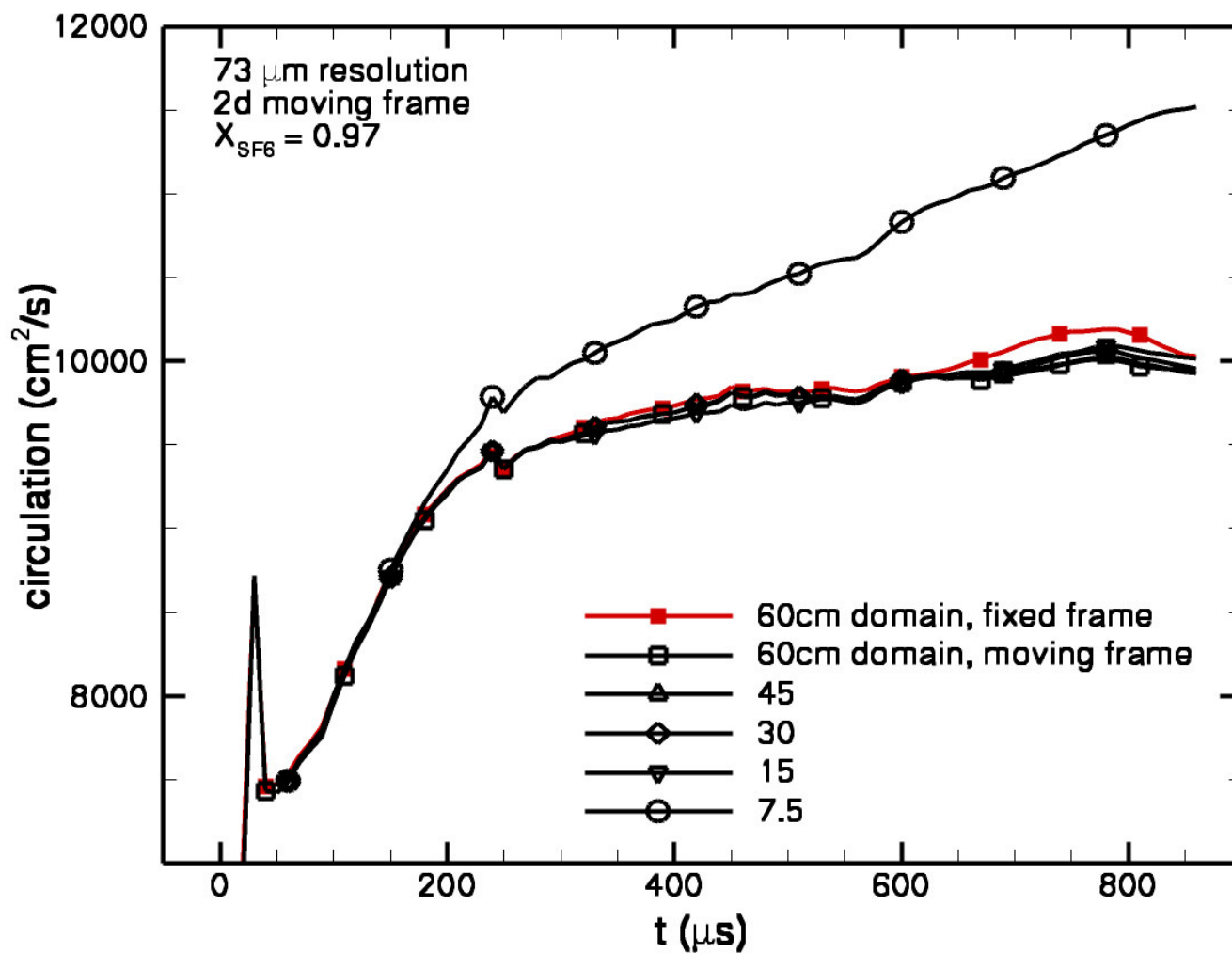
Inlet $v_z = 20.0$ cm/s



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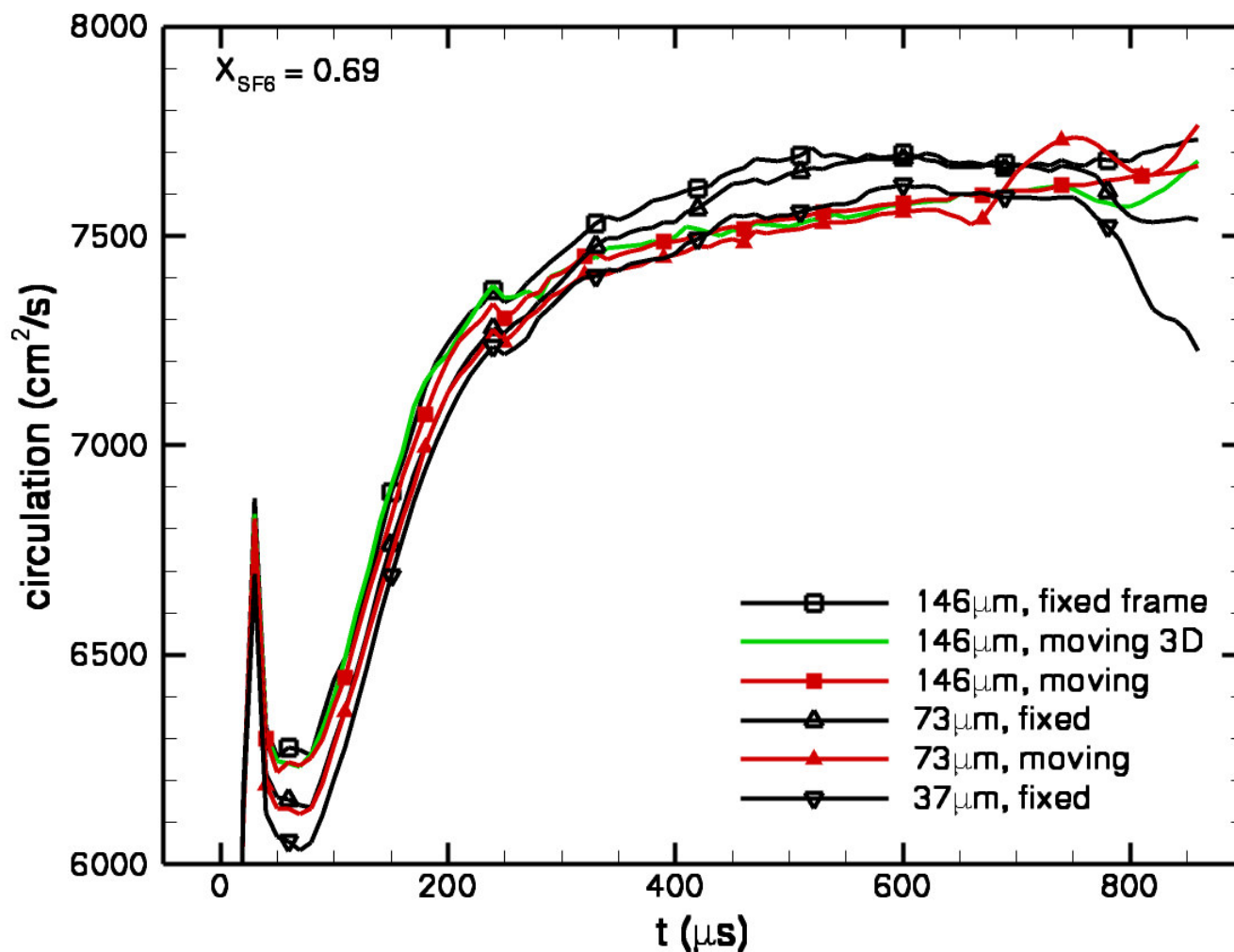
Circulation: Effect of Domain Size



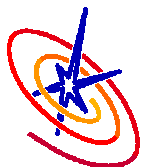
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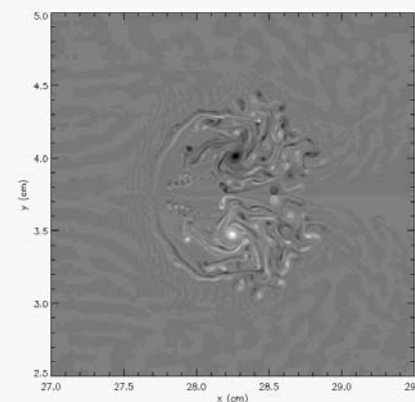
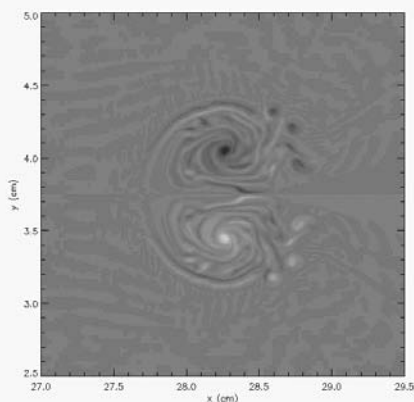
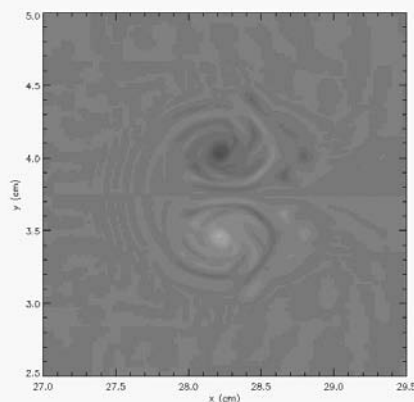
Circulation: Effects of Resolution and Ref. Frame



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Vorticity: Effects of Resolution and Ref. Frame



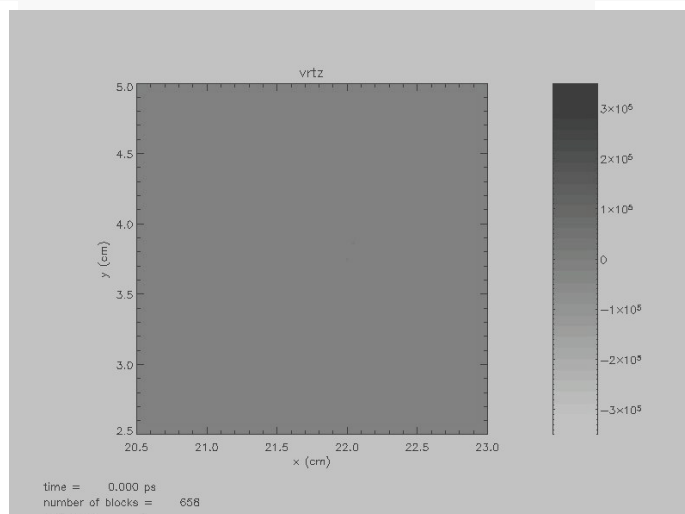
$$X_{\text{SF}_6} = 0.69$$

$$t = 750 \mu\text{s}$$

146 μm , 73 μm , 37 μm

Fixed frame (upper row)

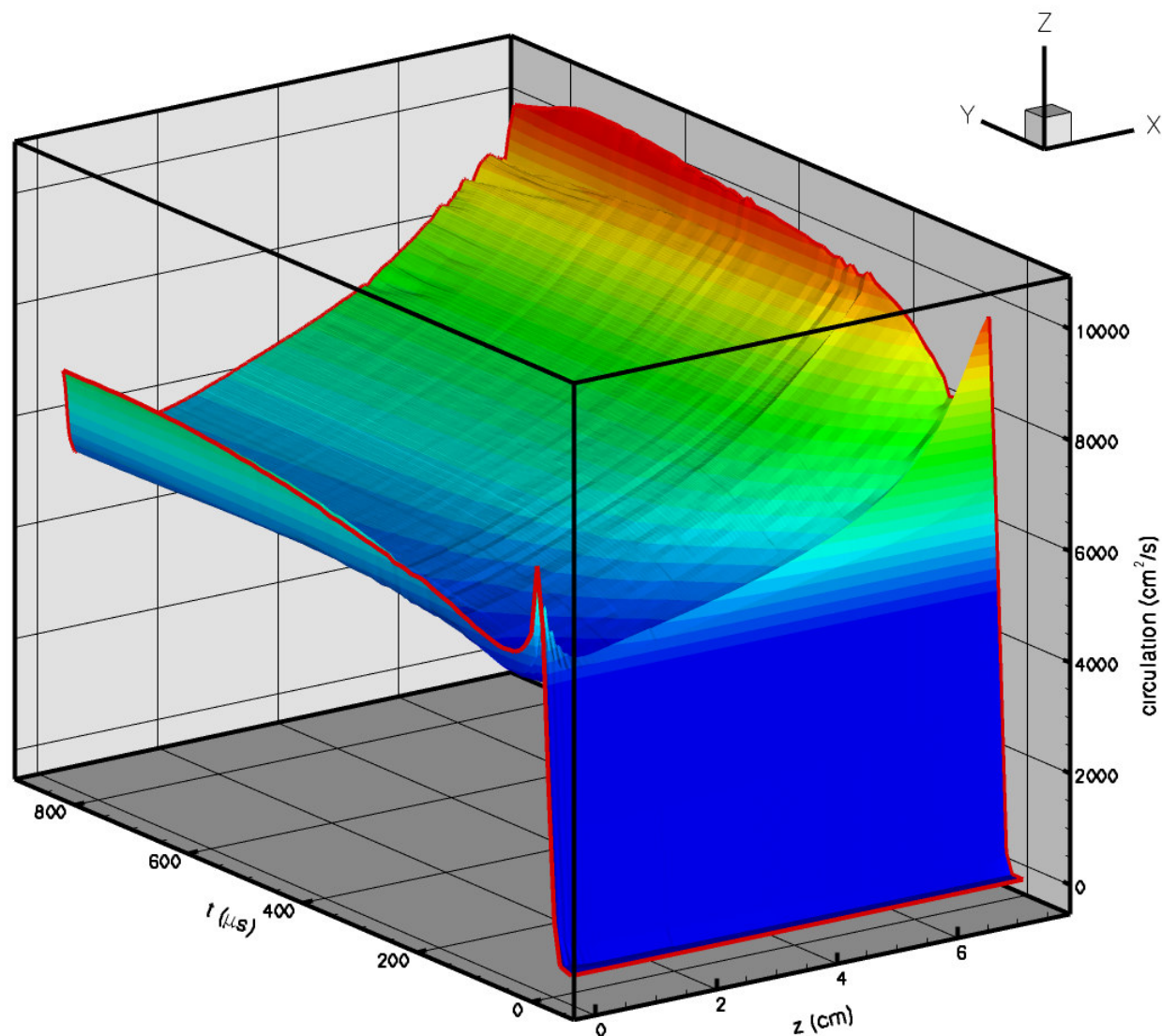
Moving frame (lower)



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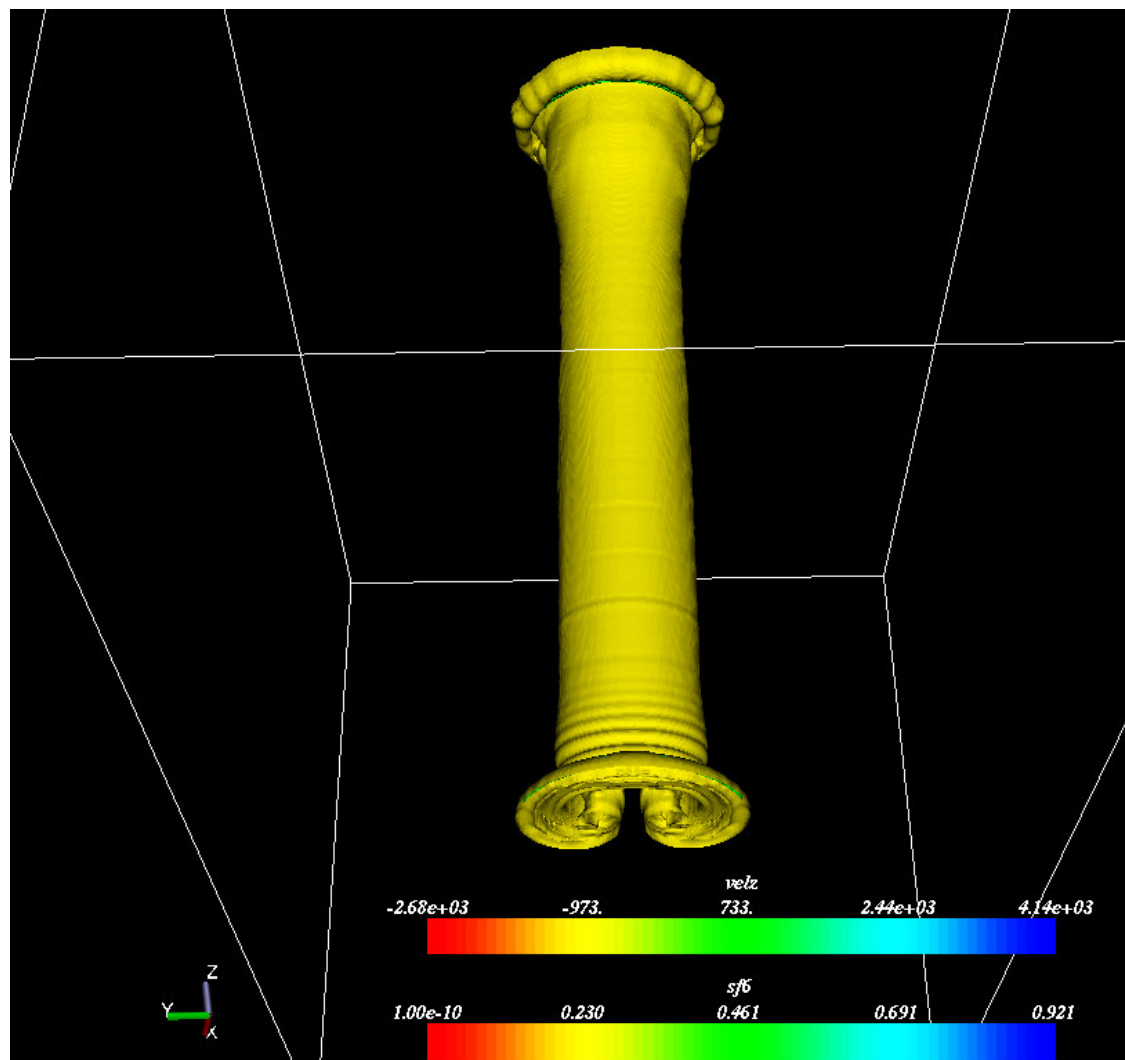
3D Simulation: Circulation



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3D Simulation: Flow Visualization



$$X_{\text{SF}_6} = 0.69$$

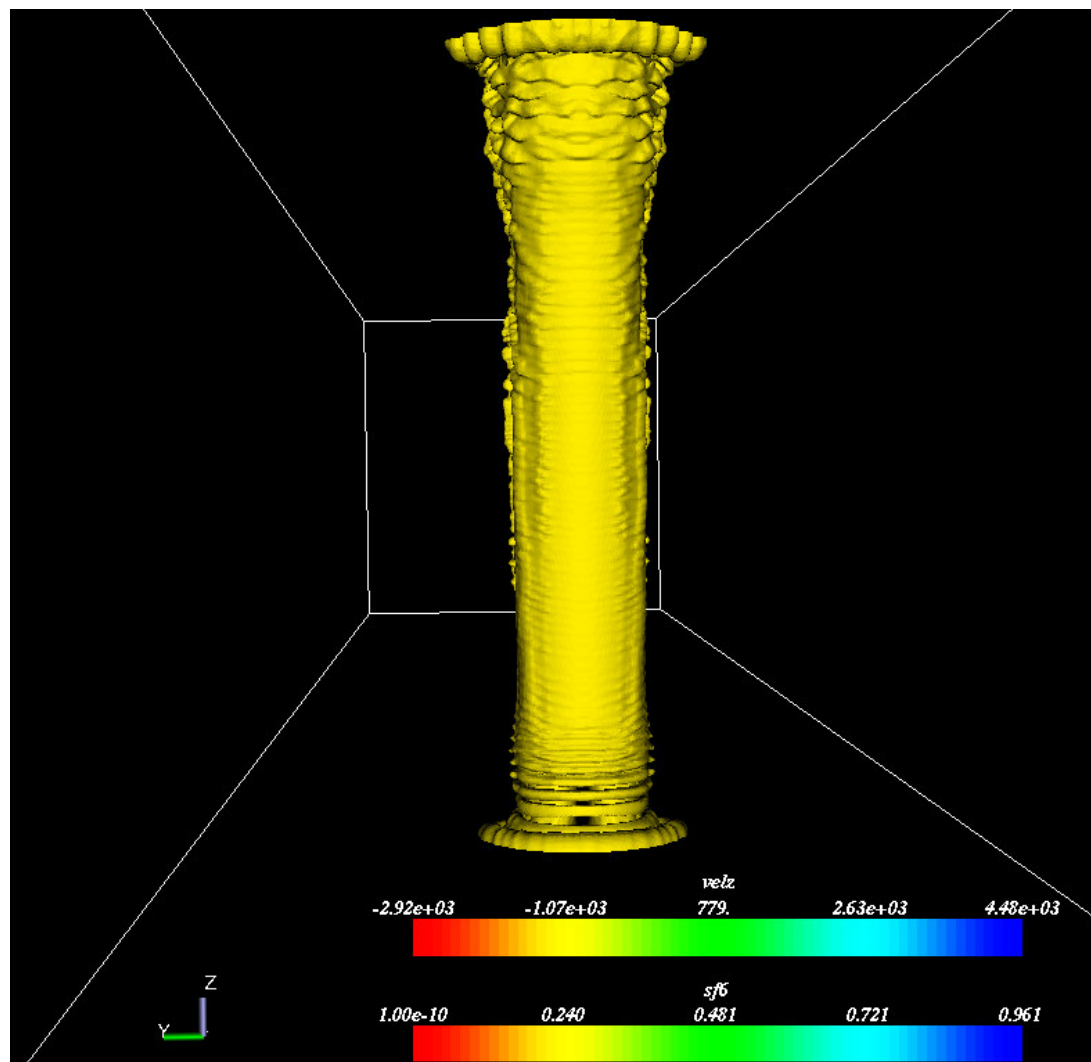
$$t = 750 \mu\text{s}$$

Front of cylinder is smooth; instabilities are not apparent

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3D Simulation: Flow Visualization



$$X_{\text{SF}_6} = 0.97$$

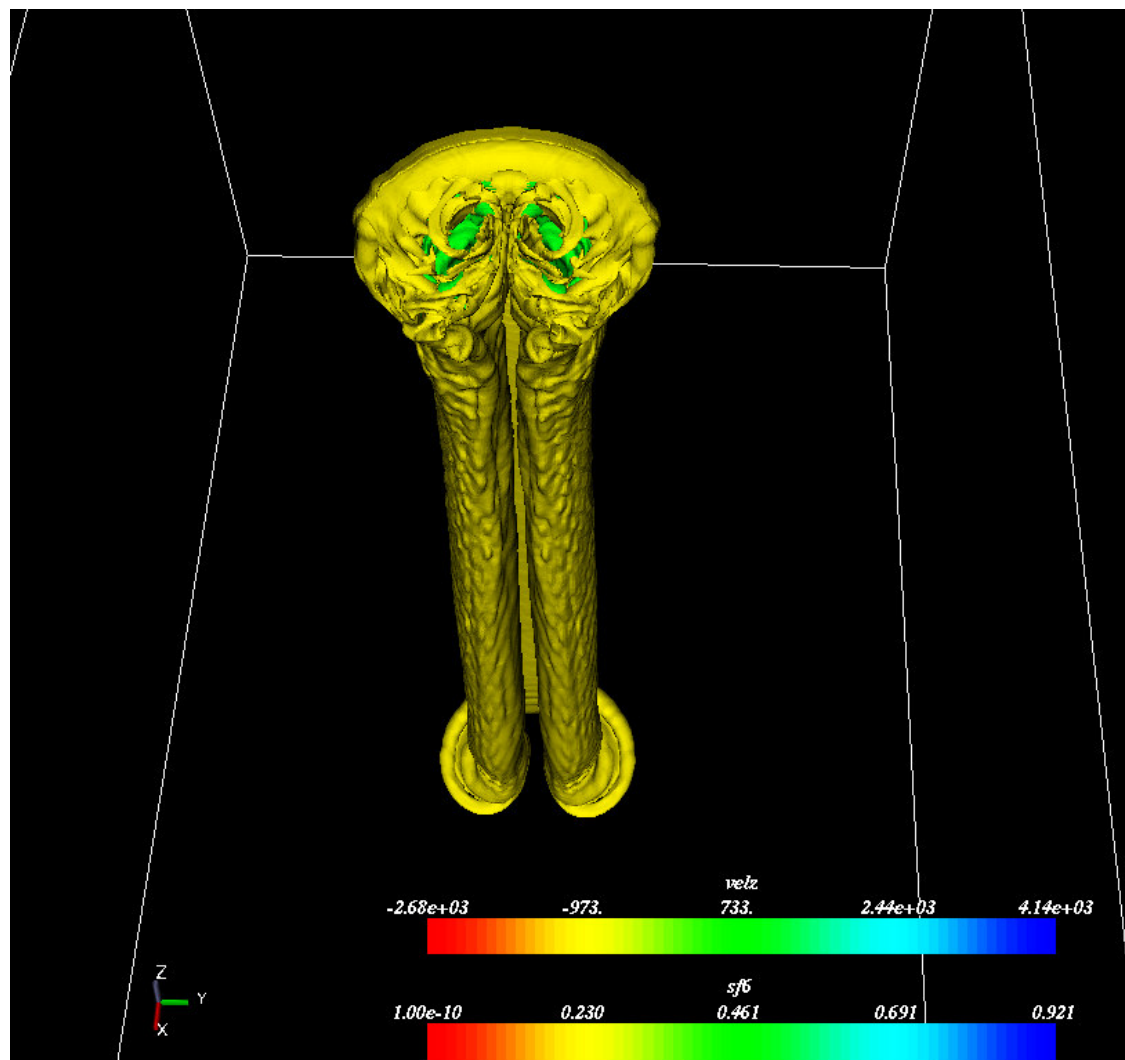
$$t = 750 \mu\text{s}$$

Instabilities are visible even on the front of the cylinder

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3D Simulation: Flow Visualization



$$X_{\text{SF}_6} = 0.69$$

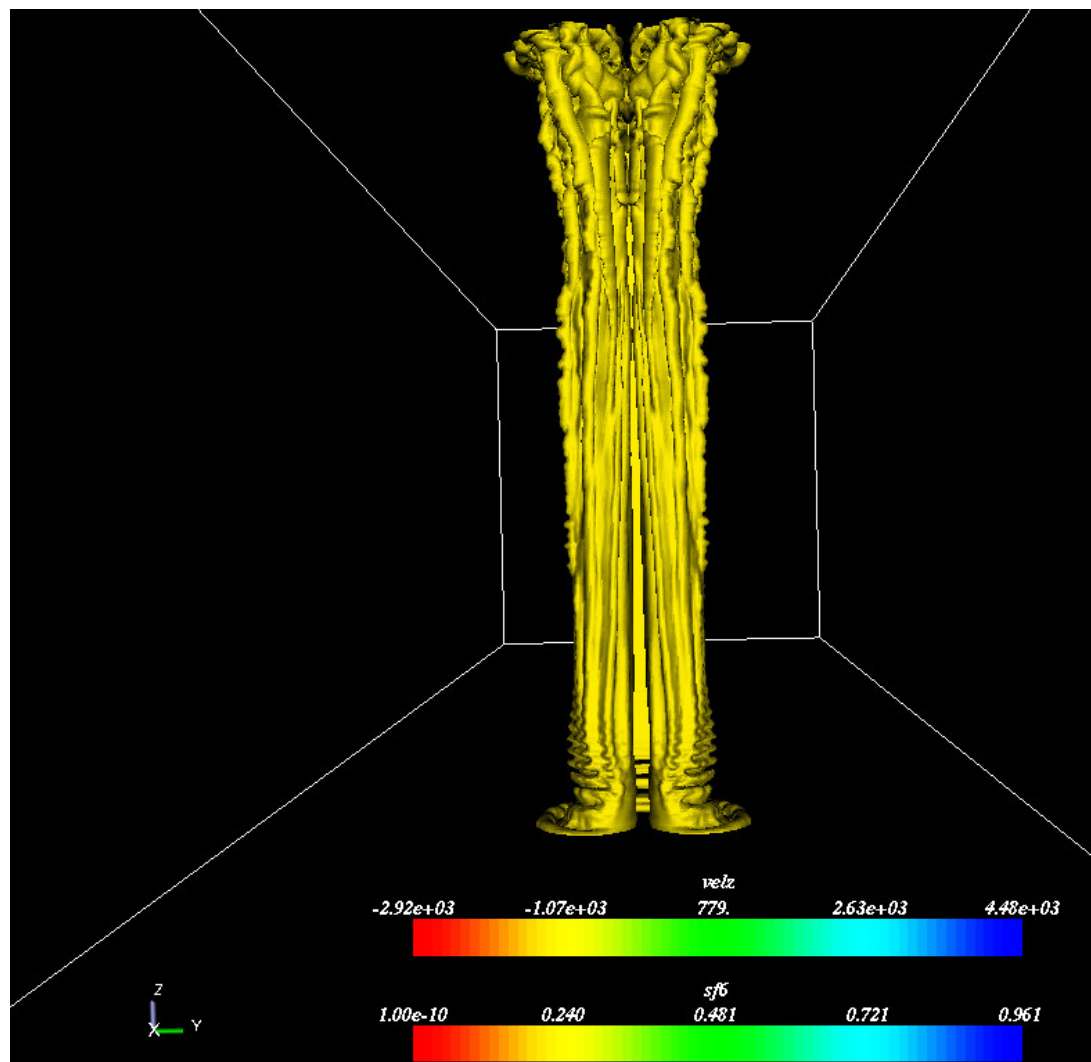
$$t = 750 \mu\text{s}$$

Mild structures are visible on the back of the cylinder

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The University of Chicago



3D Simulation: Flow Visualization



$$X_{\text{SF}_6} = 0.97$$

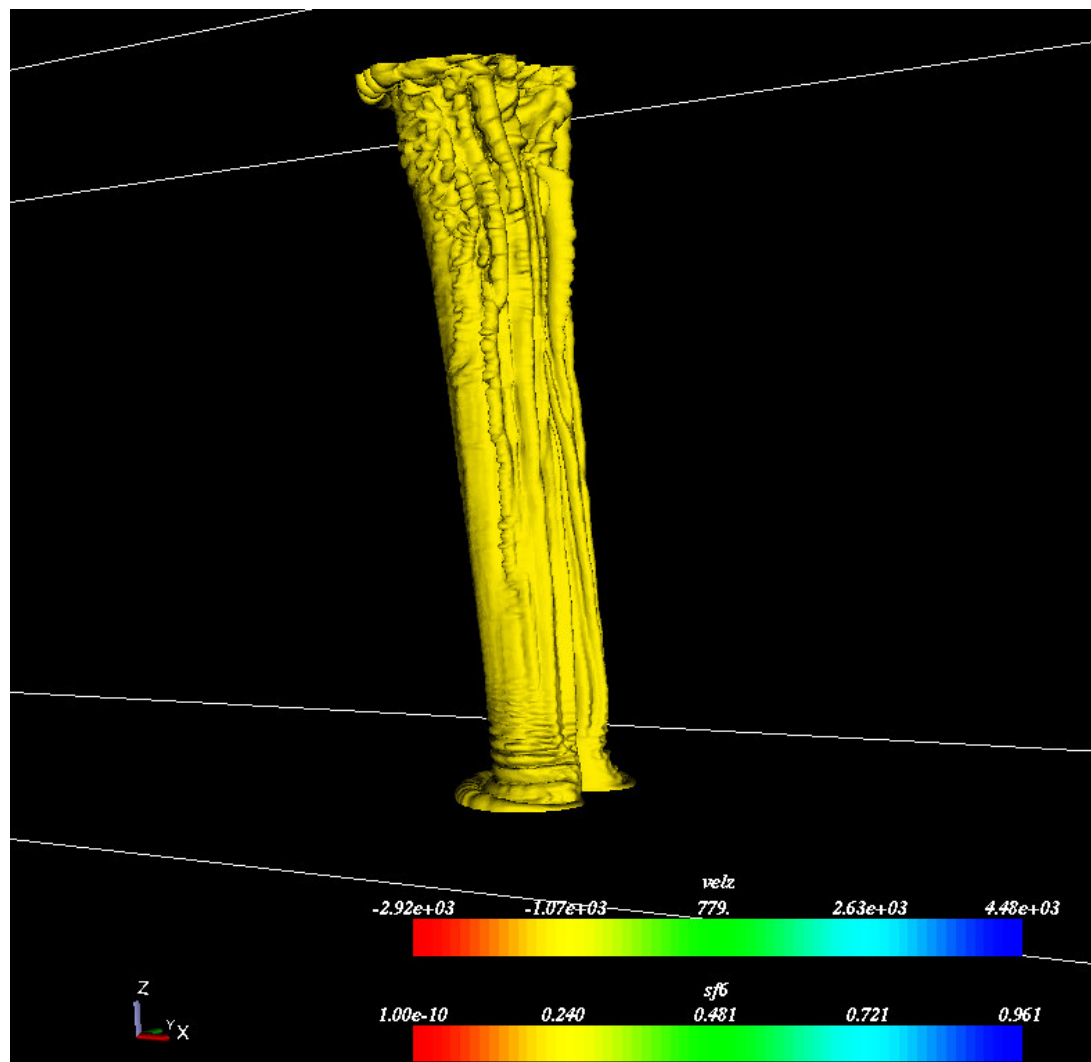
$$t = 750 \mu\text{s}$$

Well-developed structures are visible on the back of the cylinder

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3D Simulation: Flow Visualization



$$X_{\text{SF}_6} = 0.97$$

$$t = 750 \mu\text{s}$$

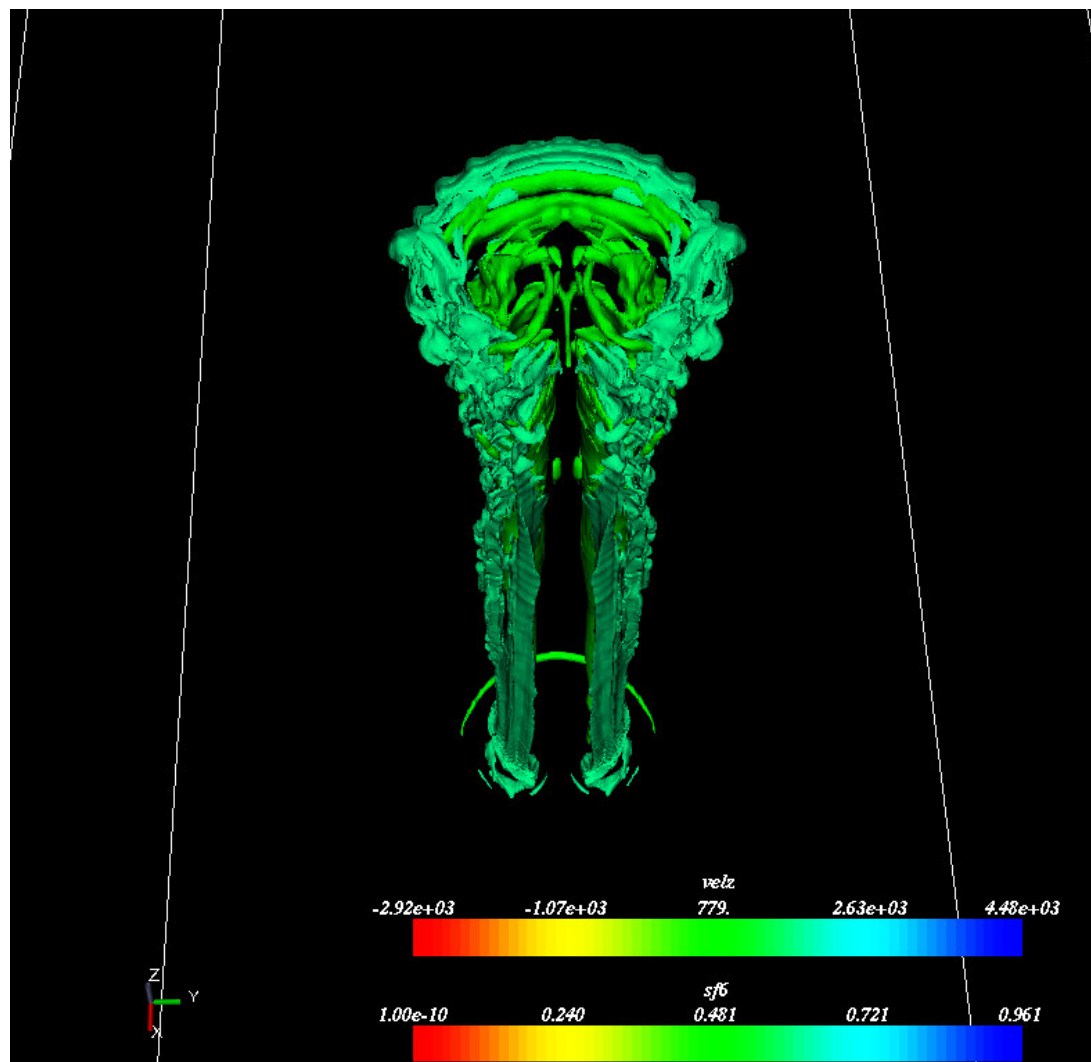
More structure is visible near the top wall than the bottom

The top of the cylinder has a higher self-induced velocity, resulting in a slight tilt

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3D Simulation: Flow Visualization



$$X_{\text{SF}_6} = 0.97$$

$$t = 750 \mu\text{s}$$

Note vertical tubes of positive z-velocity, associated with the two primary vortex cores

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