



MEASUREMENTS WITHIN A RICHTMYER-MESHKOV MIXING ZONE USING A TRIPLE HOT WIRE PROBE TECHNIQUE



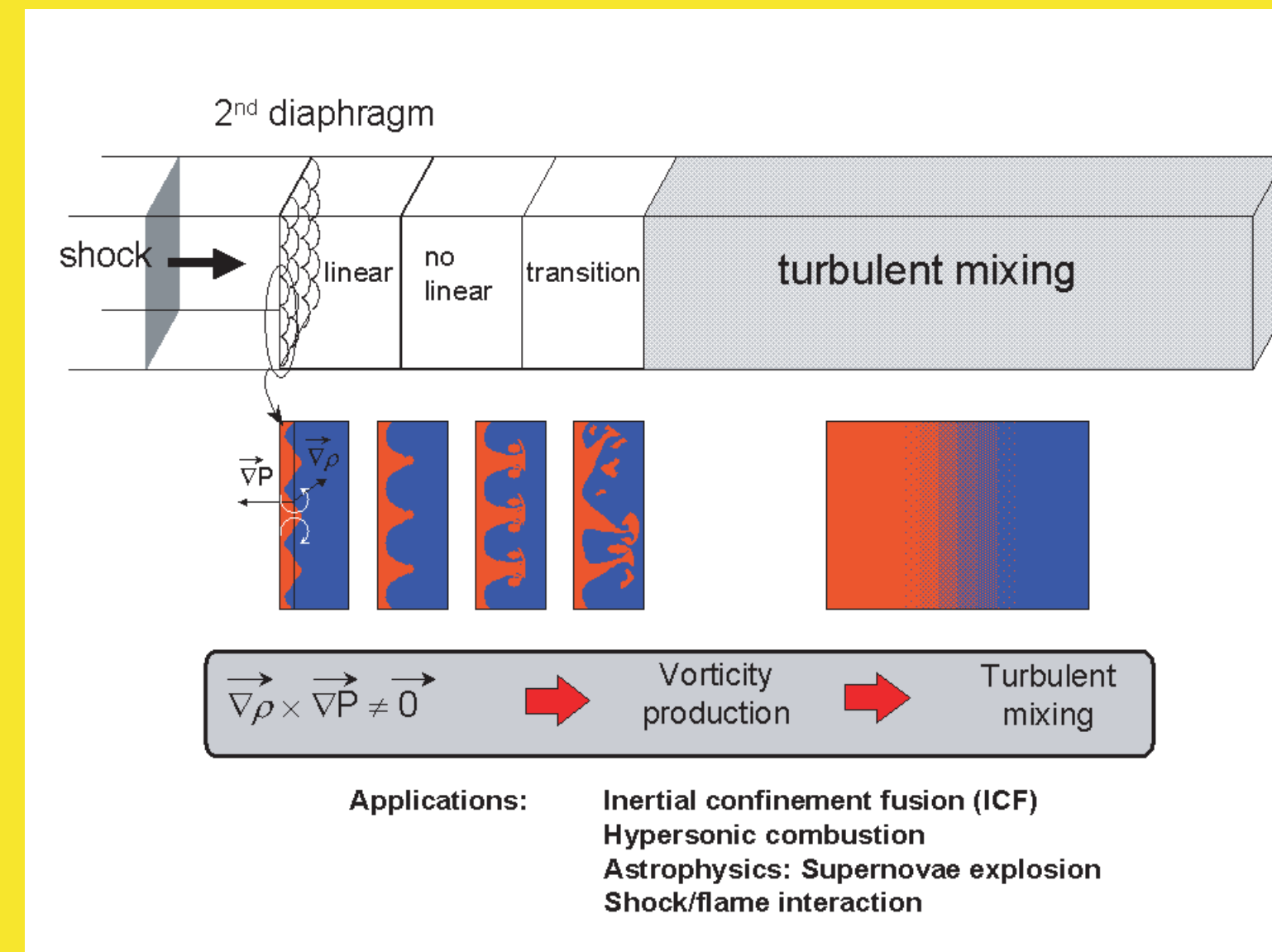
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I- INTRODUCTION

Present research topic: Characterization of a turbulent mixing zone (TMZ) induced by the Richtmyer- Meshkov instability (RMI) in a shock tube



- Global characterization : visual structures, thickness
- Time evolution of local measurements (molar fraction and velocity)
- Turbulent energy level

Schlieren visualizations

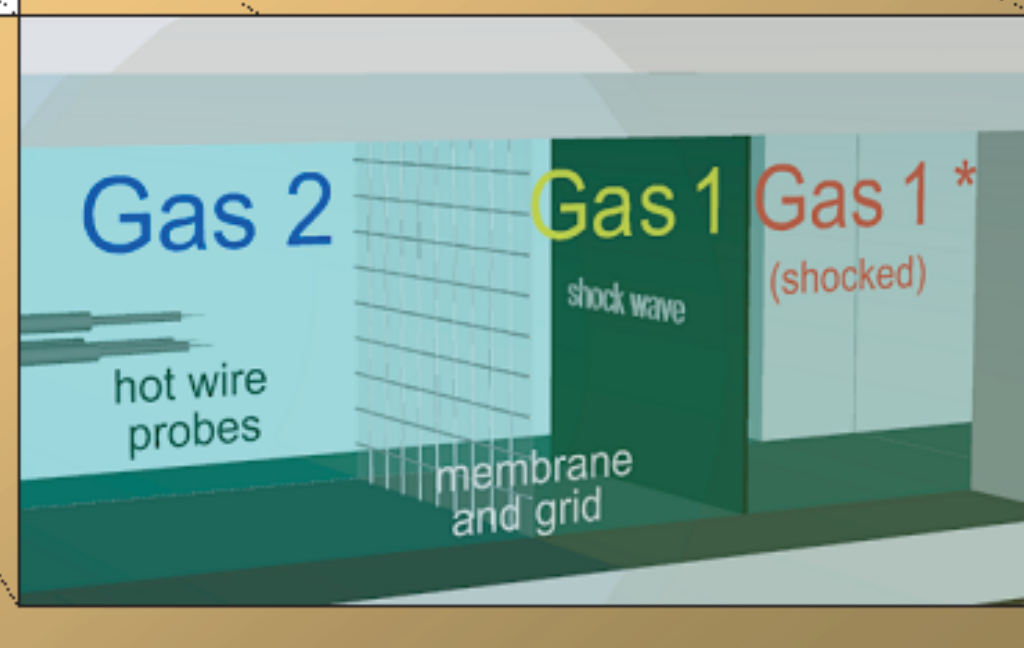
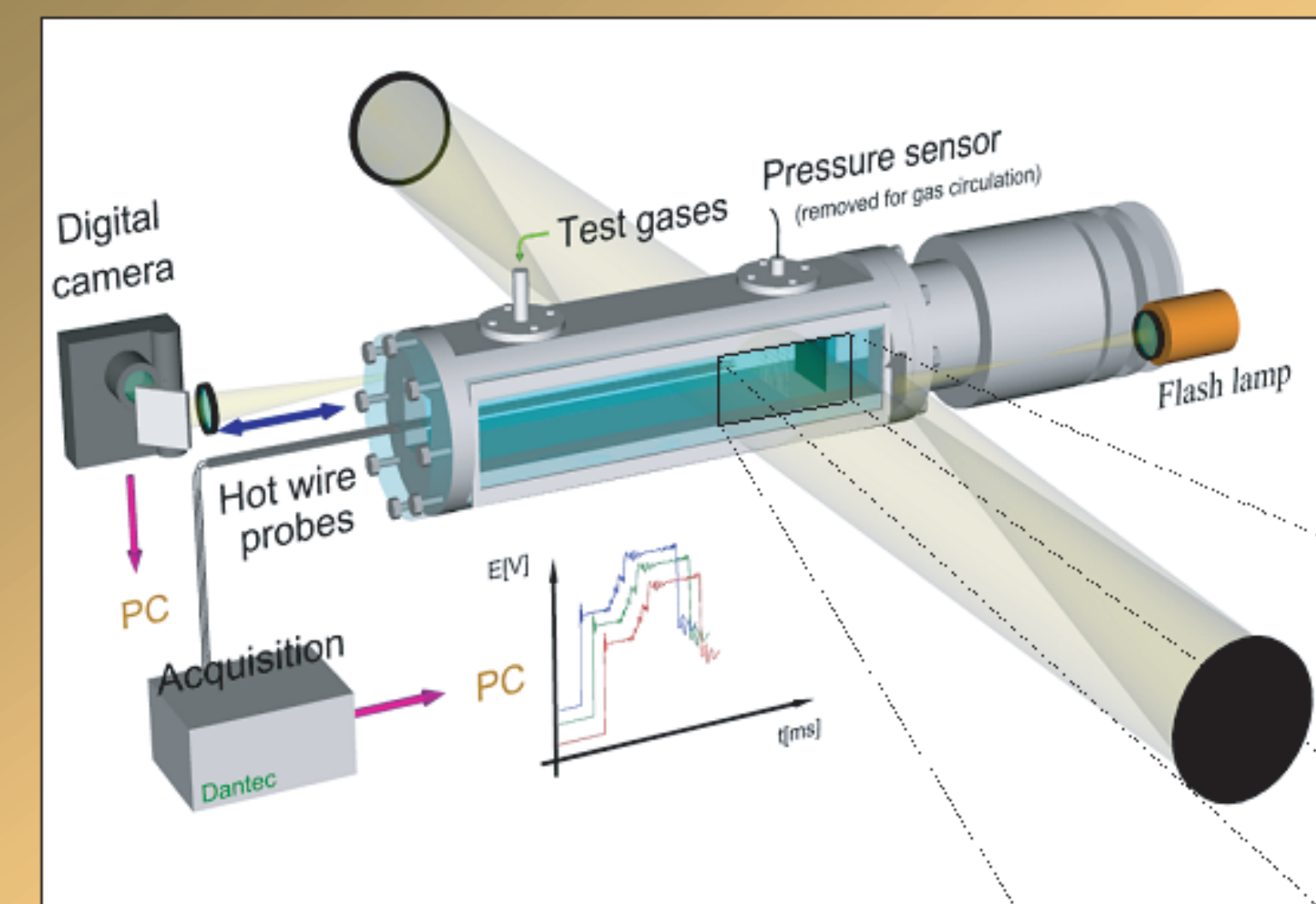
Laser Doppler anemometry (CEA/DAM)

Constant temperature hot wire anemometry (IUSTI)

II- EXPERIMENTAL SET-UP

Schlieren + Hot wire anemometry

- Constant temperature
- Single probes (5µm diam x 1.5mm length)
- Cut-off frequency : 80kHz
- Probe spacing : ~1 cm
- Sampling : 1 MHz/n probes



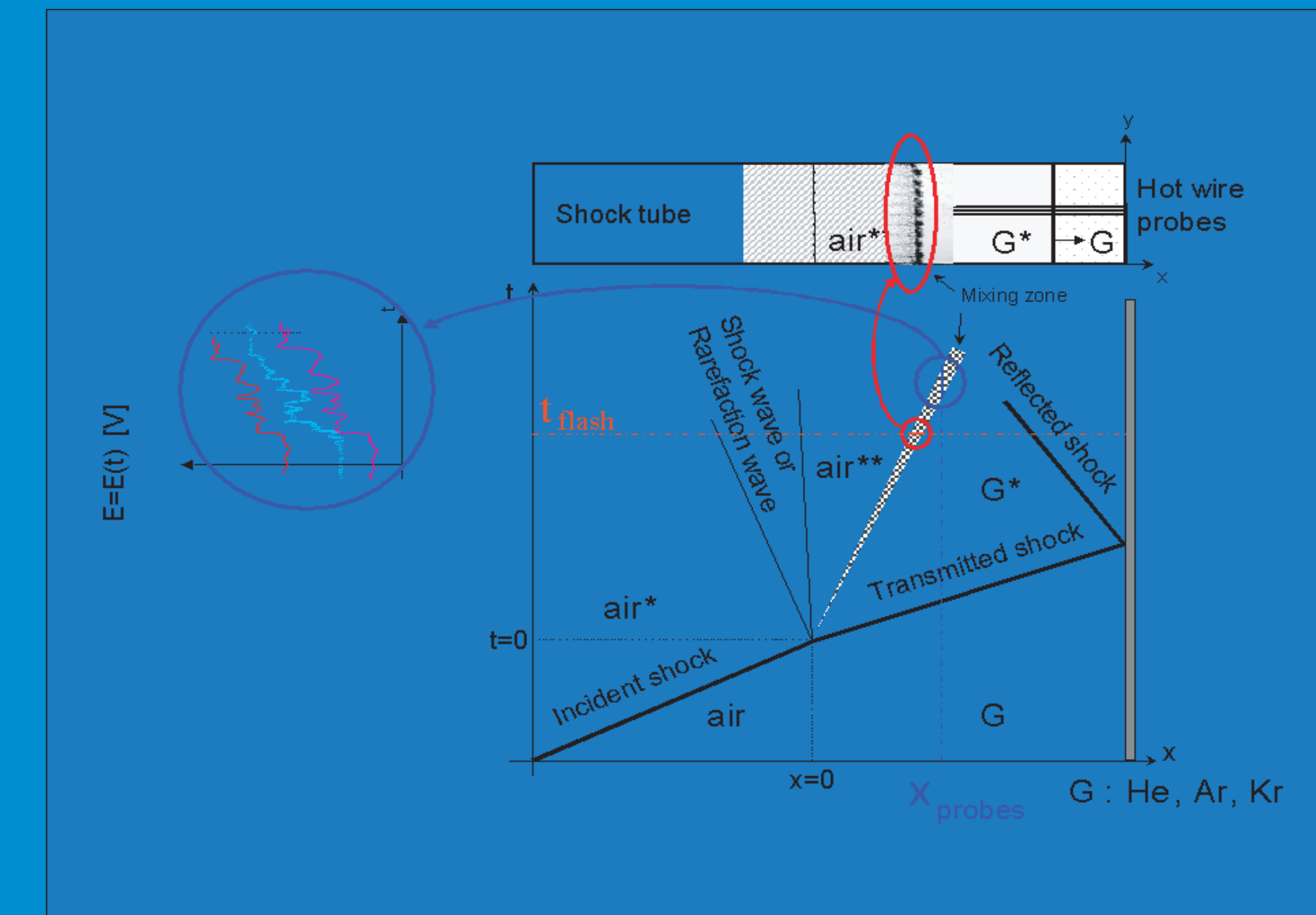
Double diaphragm shock tube

- Square cross section 85x85 mm²
- 1st diaphragm : aluminium membrane (0.8 mm thick)
- 2nd diaphragm : mylar (0.9 µm thick) or nitrocellulose (0.5 µm thick) film resting over a 100 cells or a 7225 cells grid

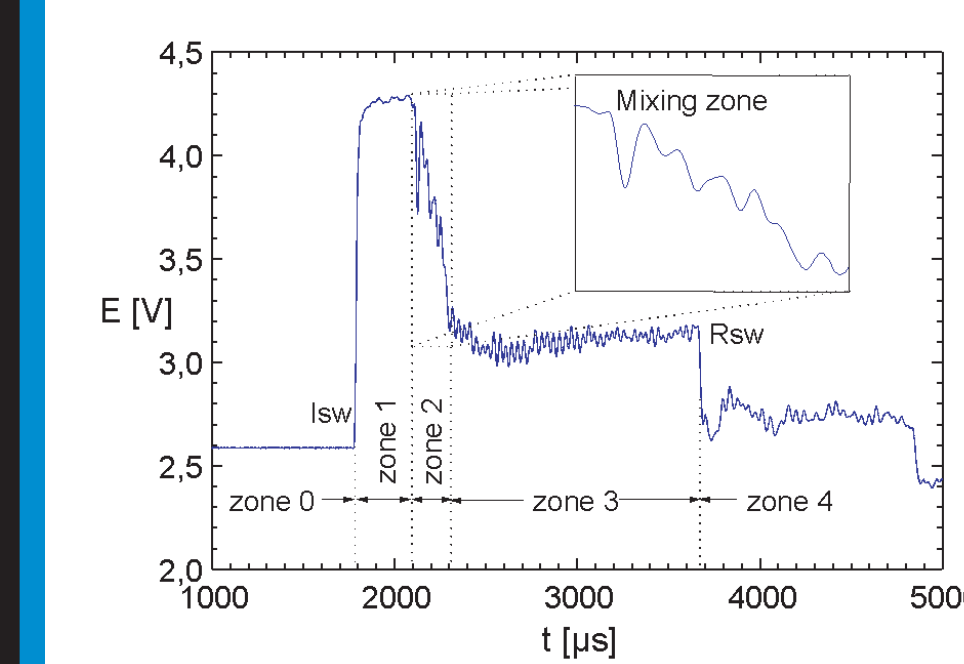
III- PRINCIPLE OF MEASUREMENTS

HWA output versus time

- Reynolds number
- species molar fraction
- velocity



Principle Heat transfer from the heated wire to the gaseous flow which depends on both the properties of the gas (μ, λ) and the parameters of the flow (U, T, ρ)



✓ *Infinitely long wire:*

$$\frac{R_w}{(R_i + R_L + R_w)^2} \frac{E^2}{T_w - T} \frac{1}{\lambda} = [0,42 \pi I Pr^{0,2}] + [0,57 \pi I Pr^{0,33}] \left(\frac{\rho U d}{\mu} \right)^{0,5}$$

$E = f(T, \rho, U, \lambda, \mu)$

E depends on both the electrical bridge data (known) and the instantaneous variations of the flow parameters

✓ *Finite length wire:*

$$\frac{R_w}{(R_i + R_L + R_w)^2} \frac{E^2}{T_w - T} \frac{1}{\lambda} = A' + B' \left(\frac{\rho U d}{\mu} \right)^n$$

A', B' and n obtained by calibration

Hypothesis: constant temperature within the mixing

⇒ $E = f(x, U, A, B, n)$

Two ways of calibration :

- graphical method (in pure and pre-mixed gases)
- direct method (A, B and n determined for each run)

⇒ $E = f(x, U)$

- resolution of the system (inverse method)

IV- INITIAL CONDITIONS

$P_{Exp} \sim 1 \text{ atm}$ $P_{LP} \sim 1 \text{ atm}$ $P_{HP} \sim 3 \text{ bars}$



$M_{is} \sim 1.32$ in air

$W_{is} \sim 460 \text{ m/s}$

Heavy/light case (air/He)

$$A_{air/He} = \frac{P_{He} - P_{air}}{P_{He} + P_{air}} = -0.7$$

$$W_{is} = 1111 \text{ m/s}$$

$$U_{mz/is} = 226 \text{ m/s}$$

$$U_{mz/rs} = 99 \text{ m/s}$$

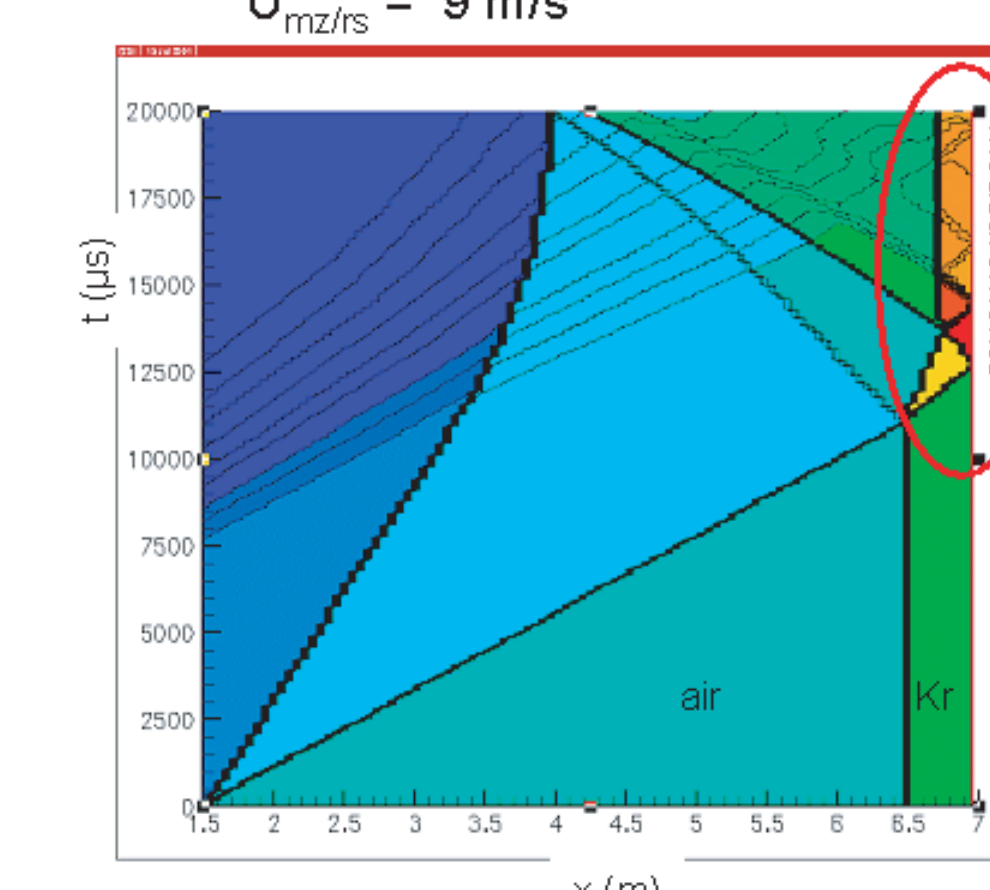
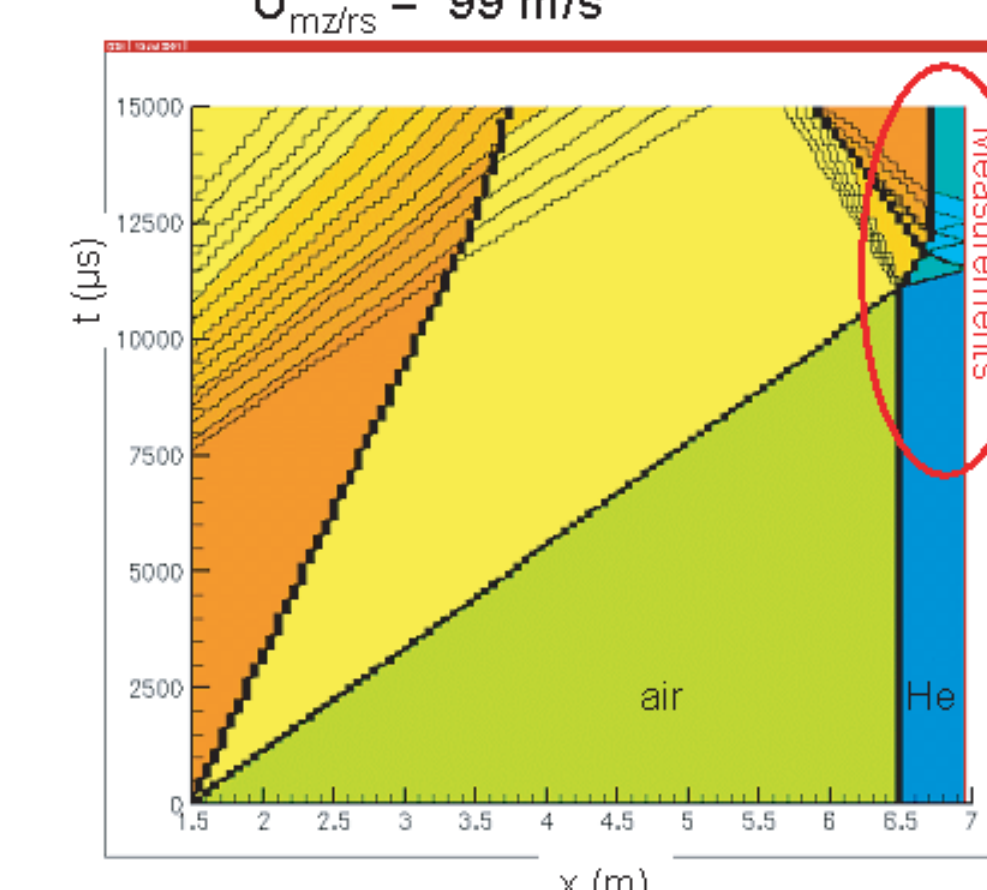
Light/heavy case (air/Kr)

$$A_{air/Kr} = \frac{P_{Kr} - P_{air}}{P_{Kr} + P_{air}} = +0.5$$

$$W_{is} = 322 \text{ m/s}$$

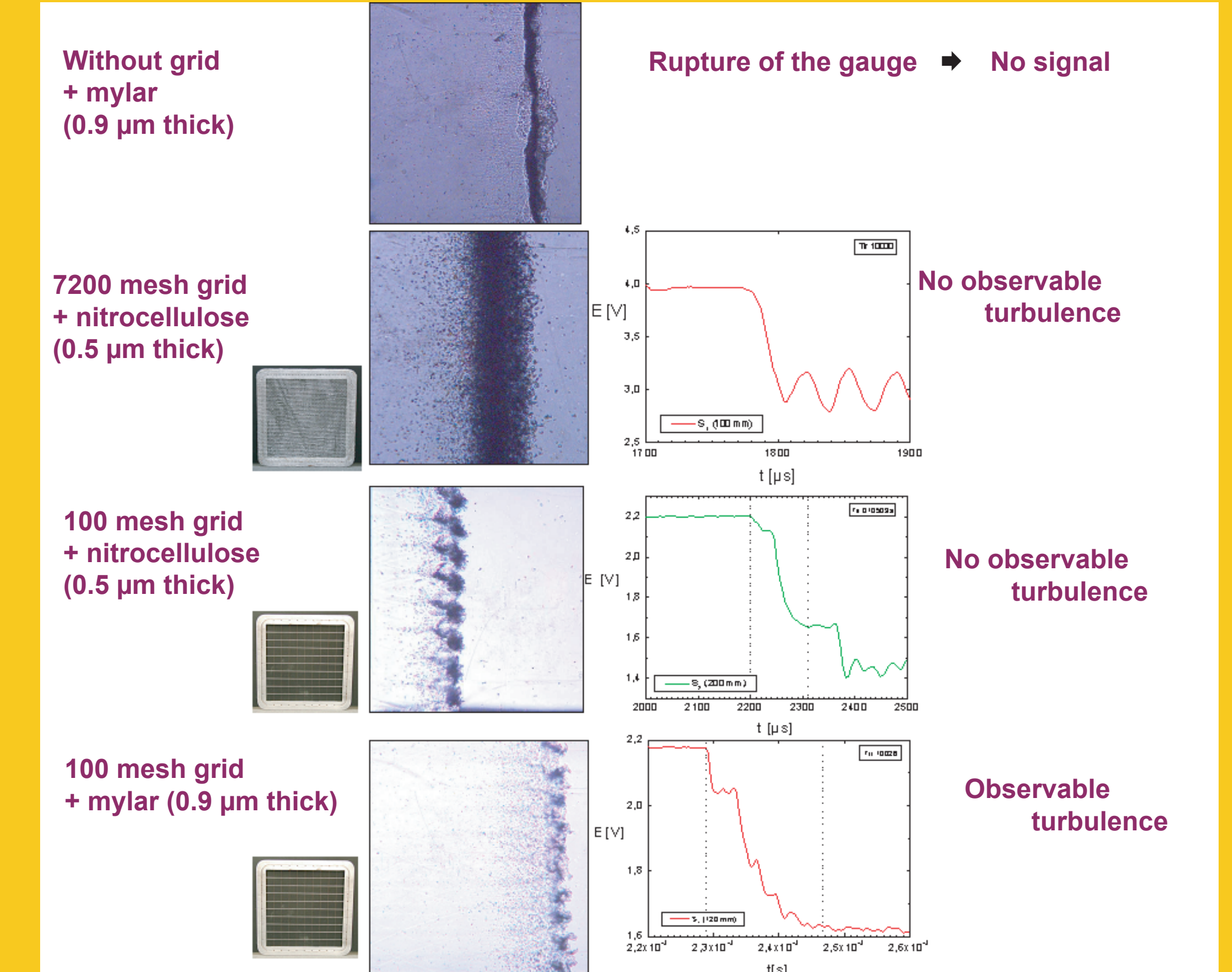
$$U_{mz/is} = 115 \text{ m/s}$$

$$U_{mz/rs} = 9 \text{ m/s}$$



V- RESULTS

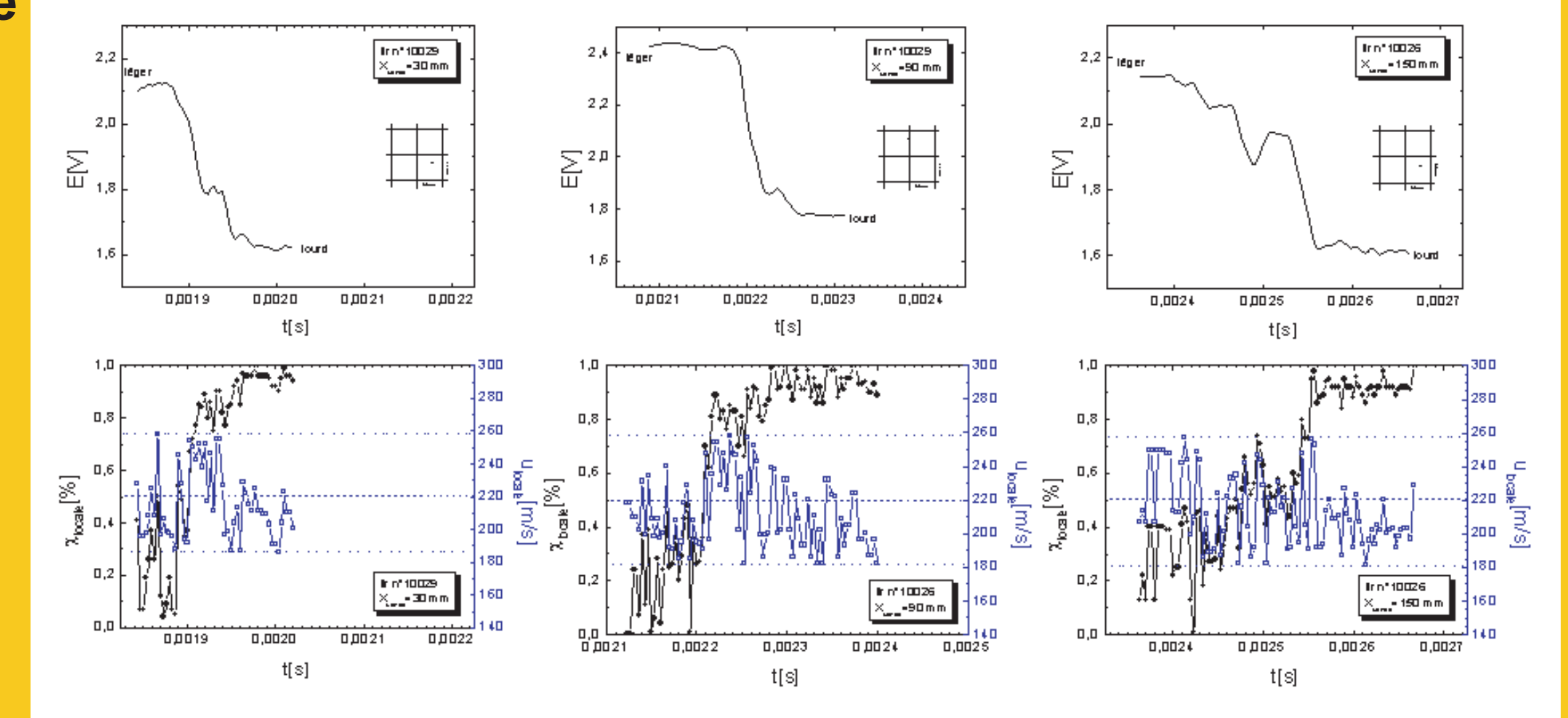
Optimal conditions



Species molar fraction and velocity profiles

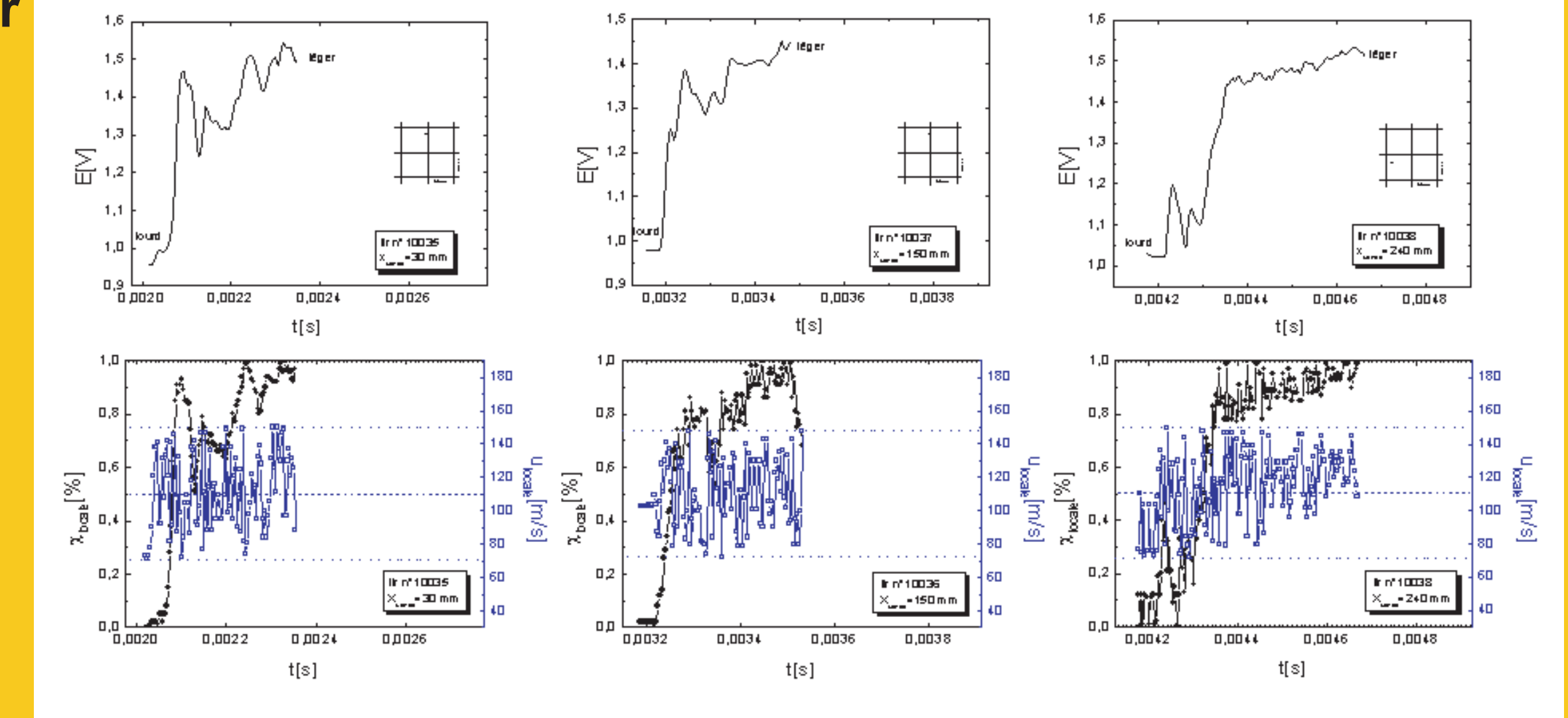
Heavy/light case

air/He



Light/heavy case

air/Kr



VI- CONCLUSION

- First exploitation of the constant temperature hot wire anemometry for the study of a turbulent mixing induced by Richtmyer-Meshkov instability in shock tube.
- Special experimental conditions have permitted the hypothesis of constant temperature within the mixing.
- Suitable calibration and signal data processes have allowed to determine the local species molar fraction and velocity within the mixing zone.