

Code-to-Code Comparisons for the Problem of Shock Acceleration of a Diffuse Dense Gaseous Cylinder

J.A. Greenough¹, W.J. Rider², C. Zoldi², J.R. Kamm²

8th IWPCTM
December 9-14, 2001
Pasadena, CA

¹Lawrence Livermore National Laboratory, ²Los Alamos National Laboratory

Motivation

- Focus on computational issues as cause for disagreement between Rage and ongoing LANL shock/cylinder experiments:
 - Large scale (dipole aspect ratio) differences
 - Quantitative velocity measurements (PIV)
- Remove experimental uncertainties/unknowns:
 - Use well-defined initial conditions
 - Analysis and comparisons based on computational data
 - Use different codes for comparison

Motivation

- Use this research to also examine:
 - What does convergence mean for evolving flows & instabilities?
 - What are the resolution requirements for “fully-resolved” calculations of this class of flow?
 - What quality of results can we obtain from low-order codes (second-order) in this regime?
- Our guide will be existing & on-going experiments

Experimental Configuration

- “Pour” SF_6 in the shocktube as a laminar stream
- LANL experiments seed gas with glycol/water droplets (original CalTech experiments used biacetyl)
- Laser sheet illumination with multiple frames per experiment

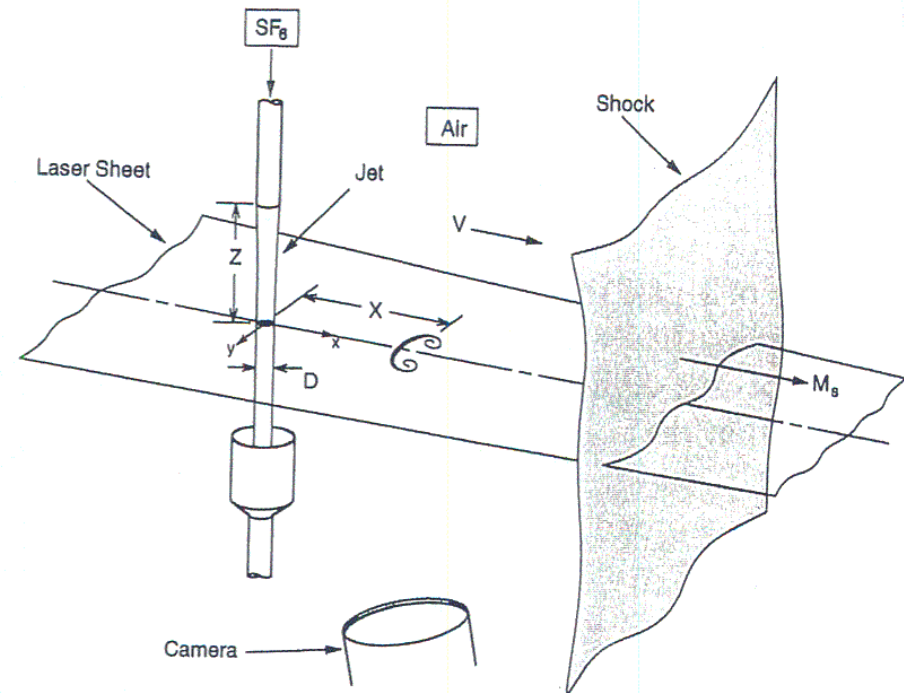
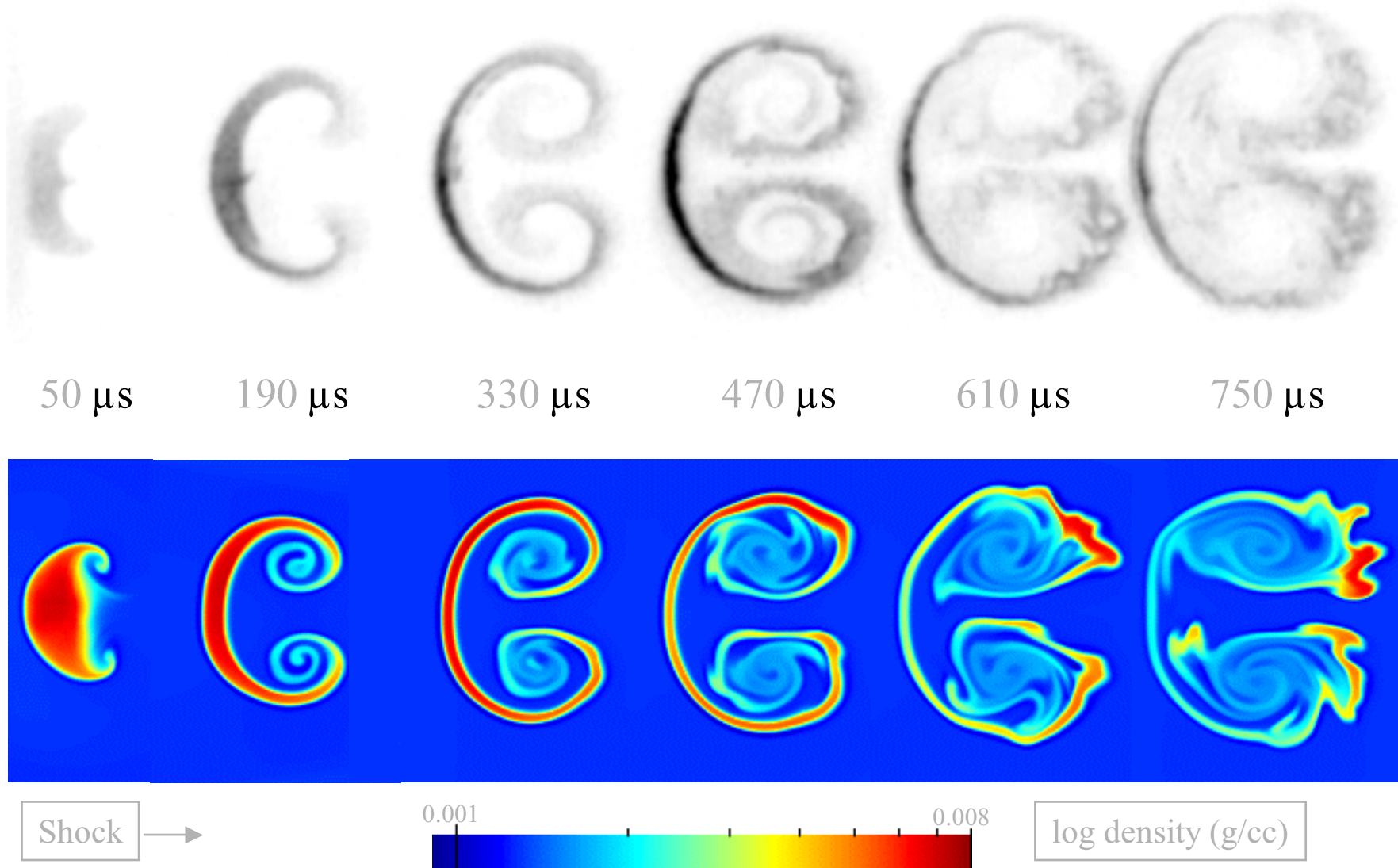
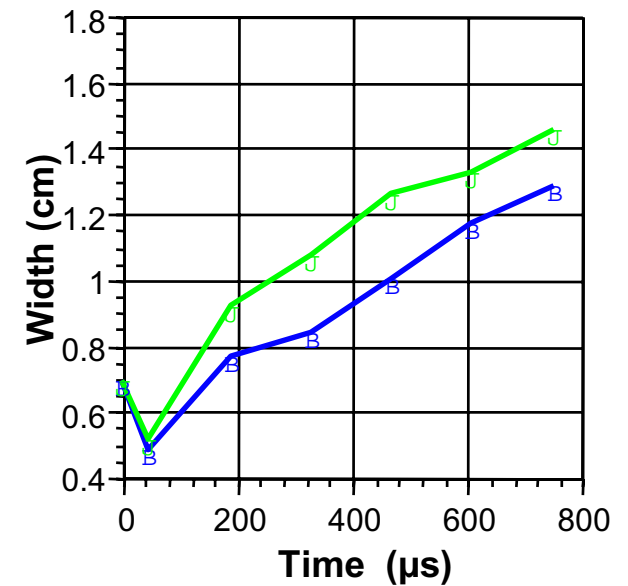
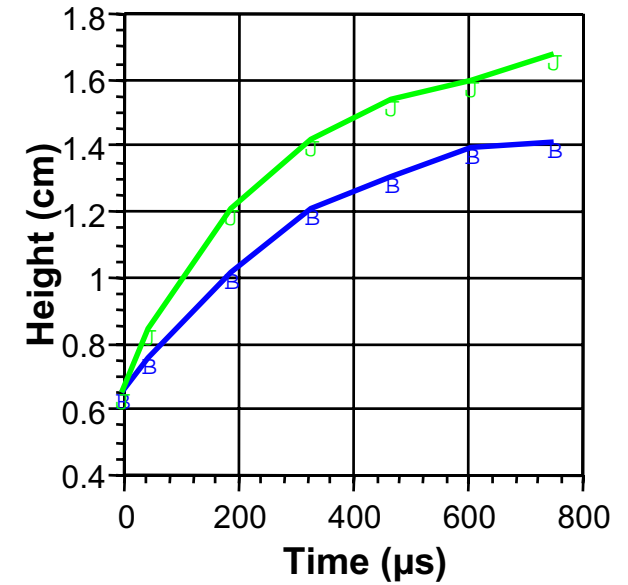
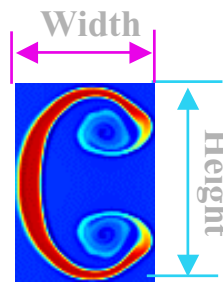
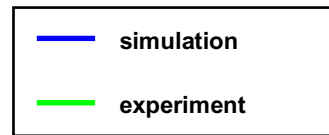
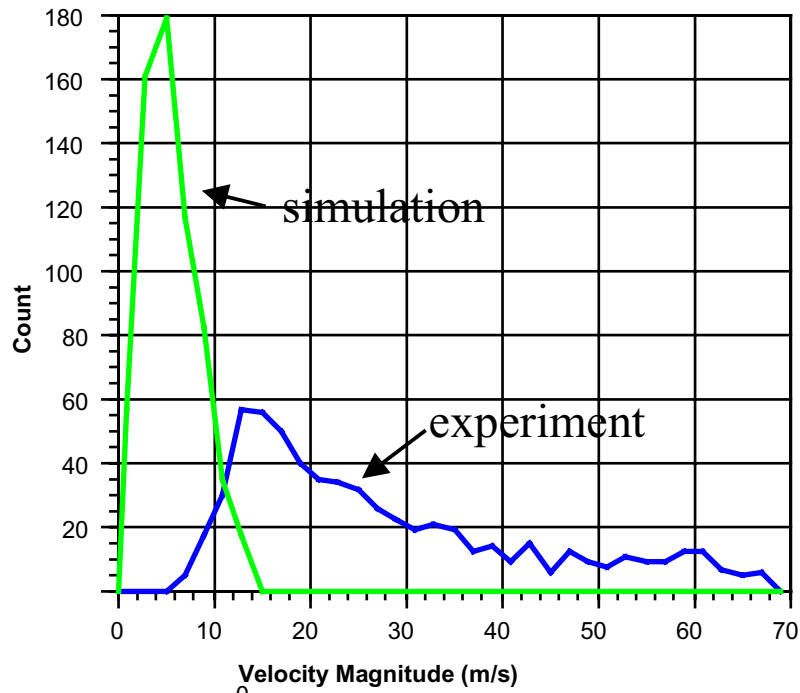


FIG. 1. Drawing of the jet/PLIF configuration.

Comparison Between Experiment and Simulation



Quantitative Measurements

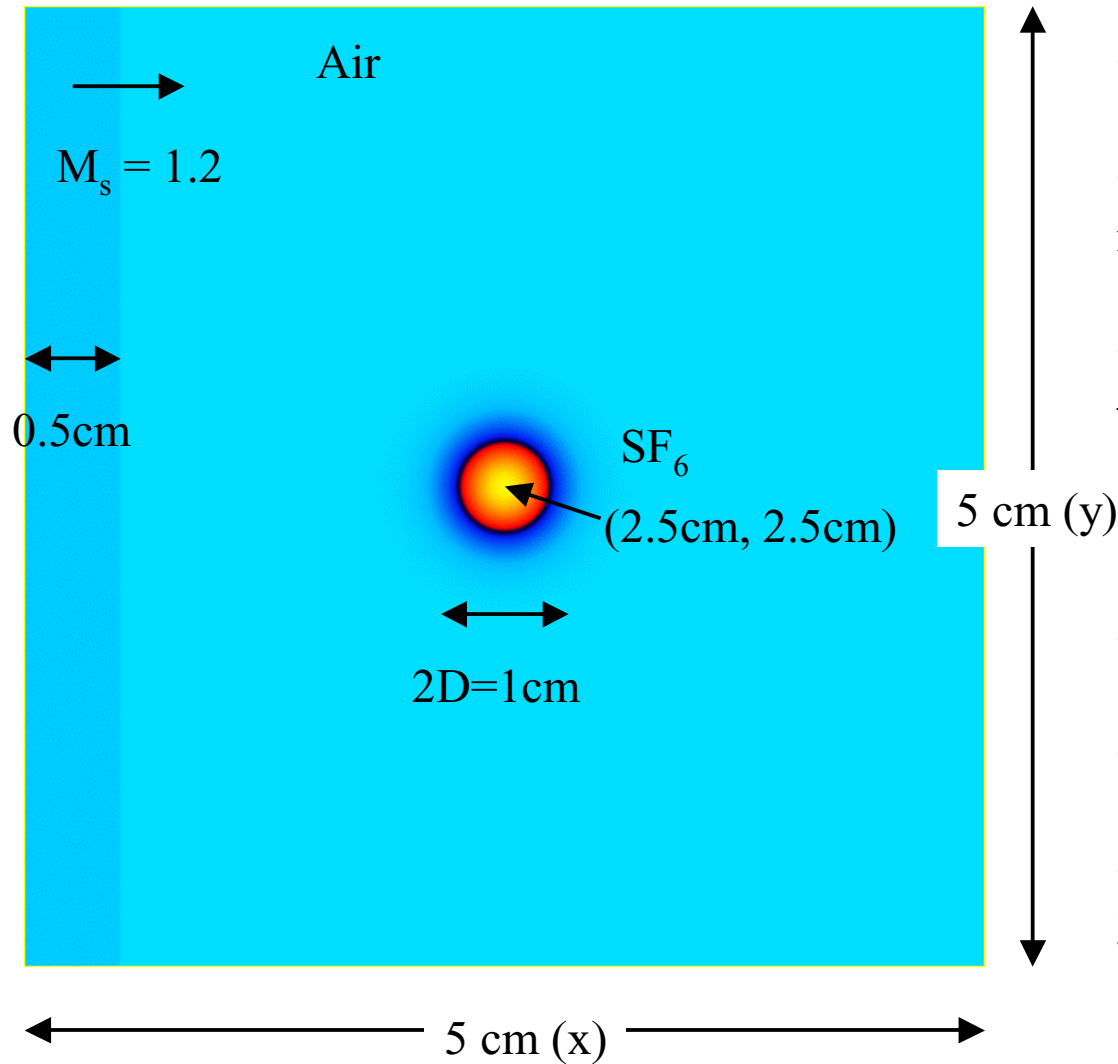


Simulation has larger velocities and smaller lengths compared to the experimental data.

Codes

- Rage (LANL; Gittings et al.)
 - Eulerian (Lagrange + Remap); directionally split
 - Unstructured AMR (point-wise adaptivity)
 - Multi-component formulation (mass fraction); one energy equation
 - Euler equations (inviscid)
- Cuervo (LANL; Rider & Kamm)
 - Eulerian (direct); directionally and temporally unsplit
 - Rectangular uniform grids
 - single-component formulation (gamma blending); one energy equation
 - Navier-Stokes equations (constant properties)
- Raptor (LLNL; Greenough et al.)
 - Eulerian (direct); directionally split
 - Block-structured AMR (patch-based adaptivity)
 - VOF formulation (volume fraction); N energy equations
 - Navier-Stokes equations (Chapman-Enskog, Sutherland's formula)

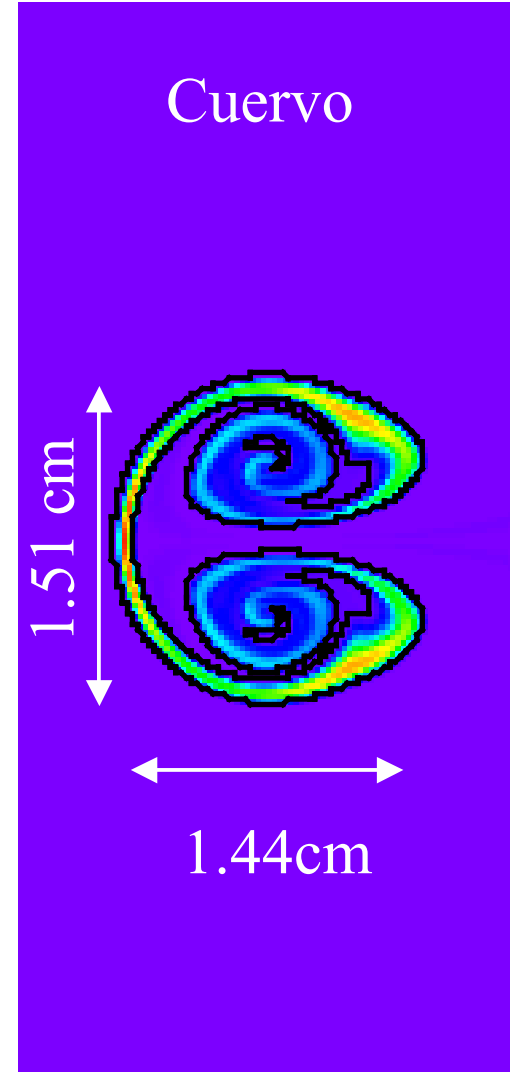
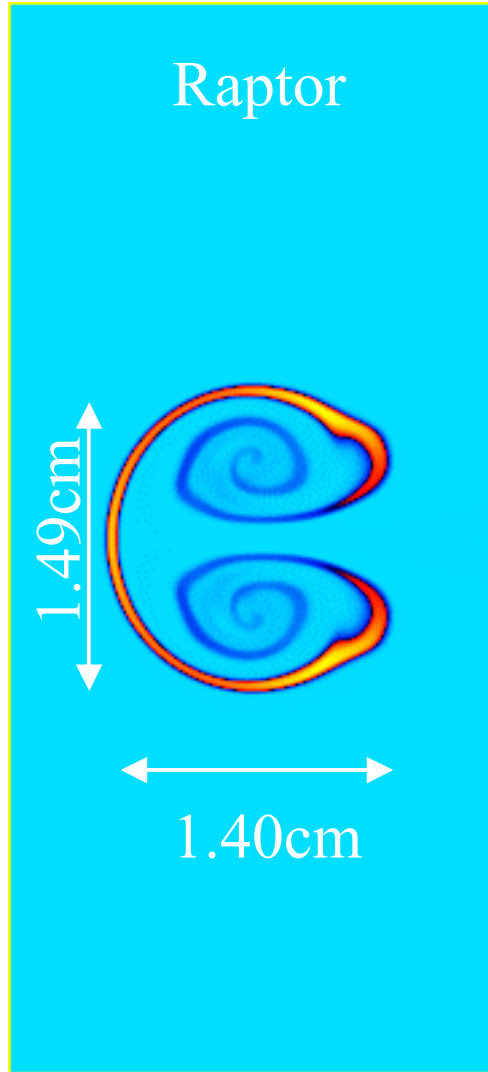
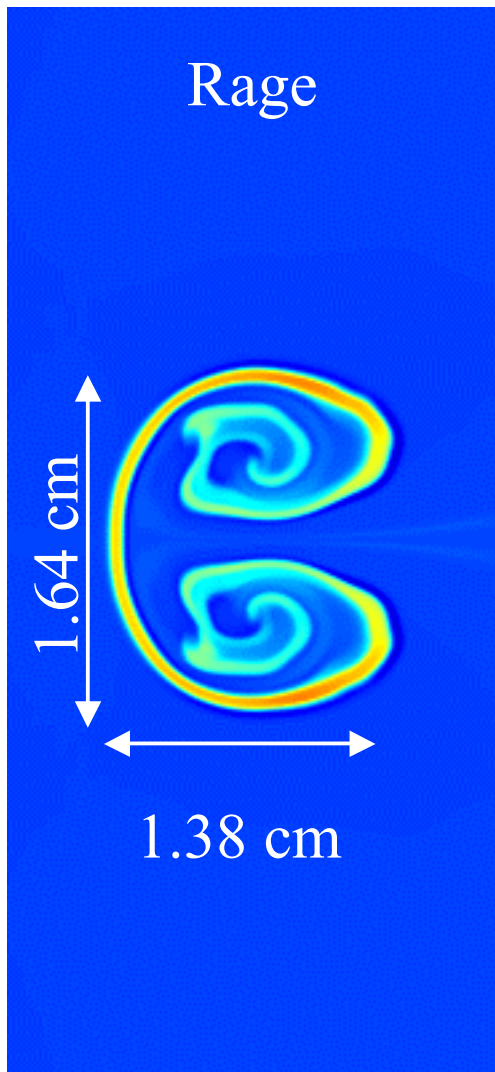
Model Problem



- Inflow/outflow B.C.'s
- Moving frame with post-interaction velocity near zero
- $\rho_{SF_6} = \rho_0 \exp(-r^2/\delta)$, $r = \sqrt{(x-x_0)^2 + (y-y_0)^2}$, $\delta = 0.0902$; $D = 0.5$ cm
- LANL pre-shock conditions
- $t_{final} = 0.8$ msec
- $\Delta x = 125\mu\text{m}, 62.5\mu\text{m}, 31.25\mu\text{m}, 15.625\mu\text{m}, 7.8125\mu\text{m}$

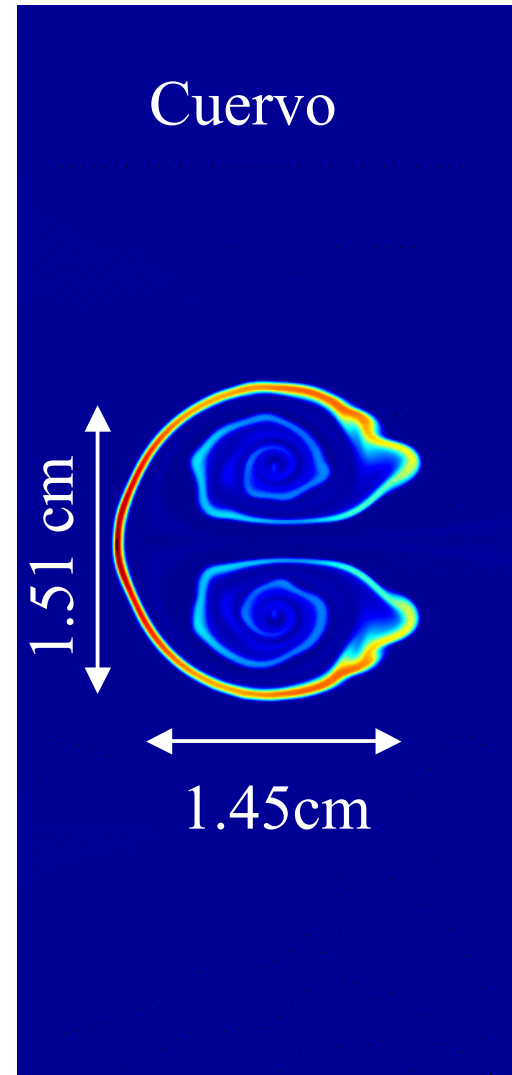
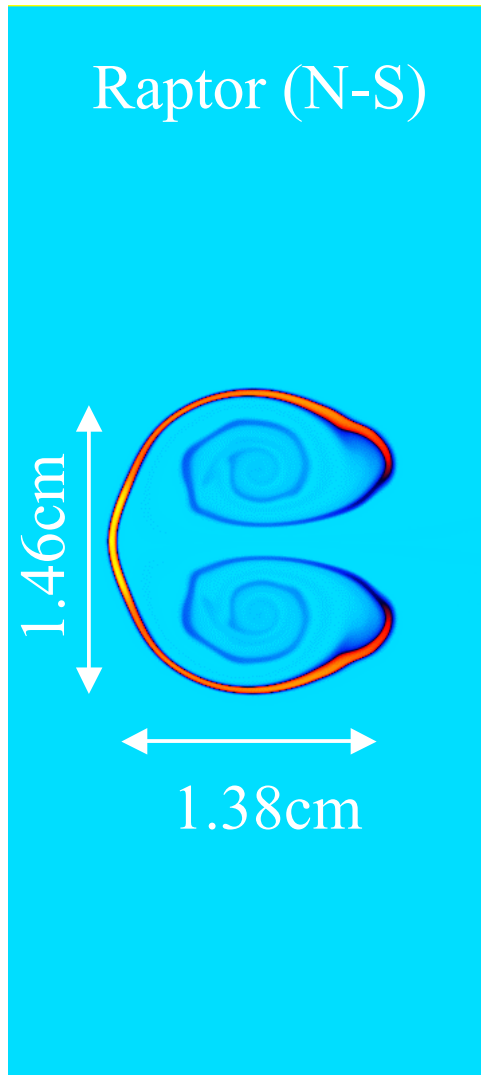
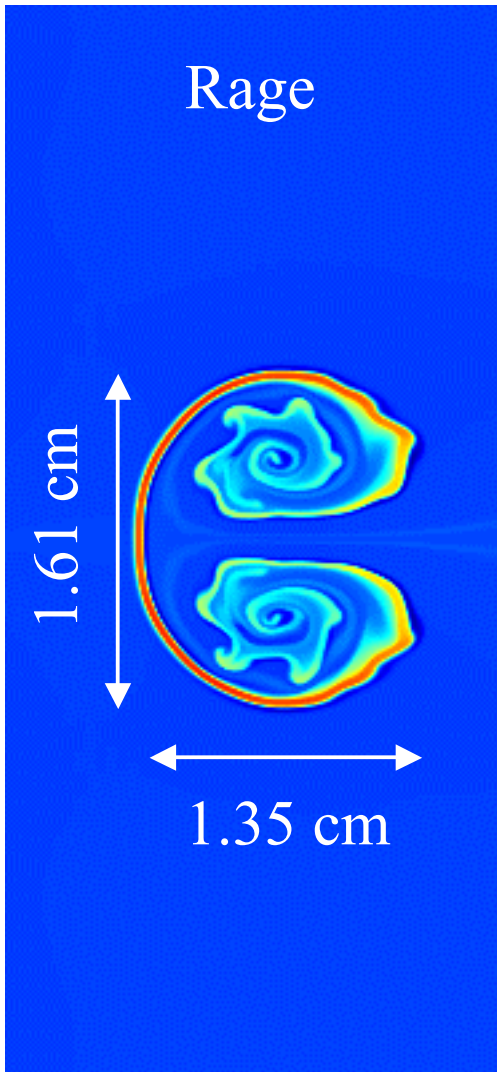
Integral Lengths/Flow

125 micron zoning, $t = 0.8$ msec



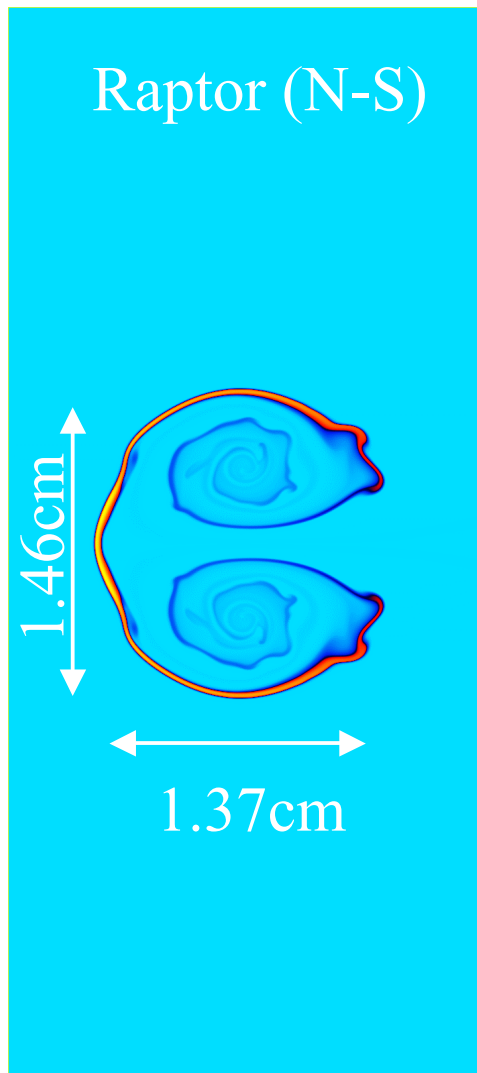
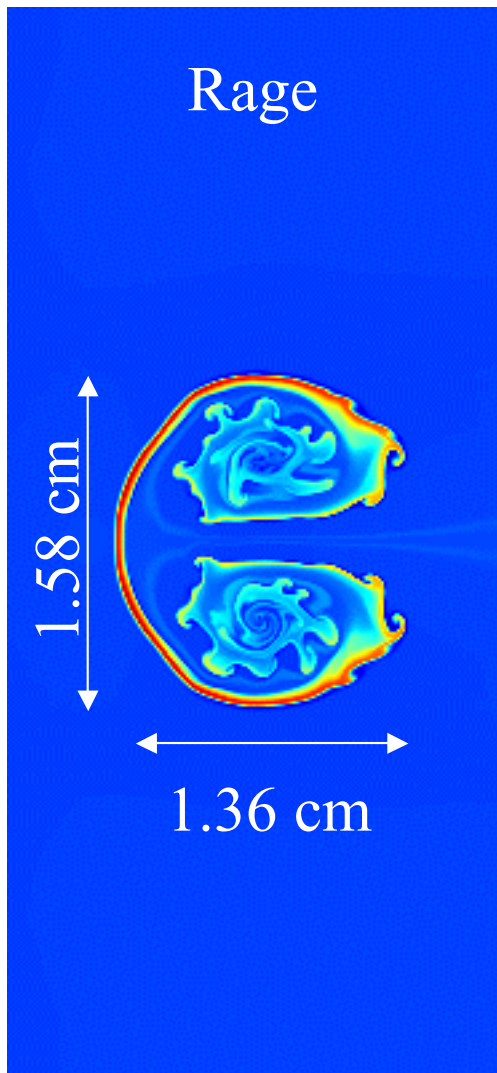
Integral Lengths/Flow

62.5 micron zoning, $t = 0.8$ msec



Integral Lengths/Flow

31.25 micron zoning, $t = 0.8$ msec

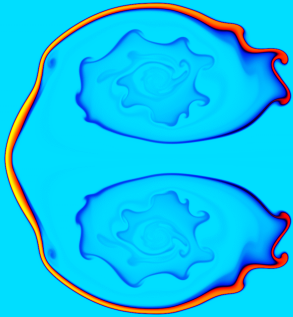


Integral Lengths/Flow

15.125 micron zoning

Raptor (N-S)

1.46cm

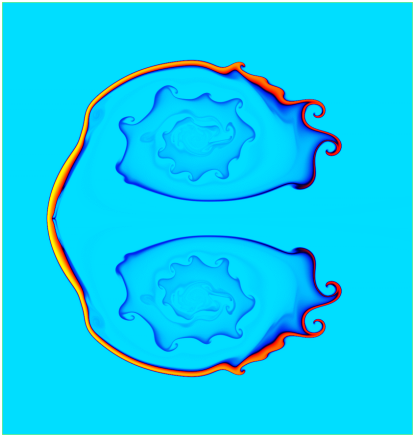


1.35cm

7.8125 micron zoning

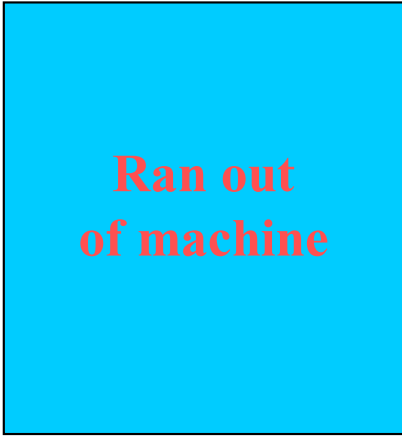
Raptor (N-S)

1.46cm

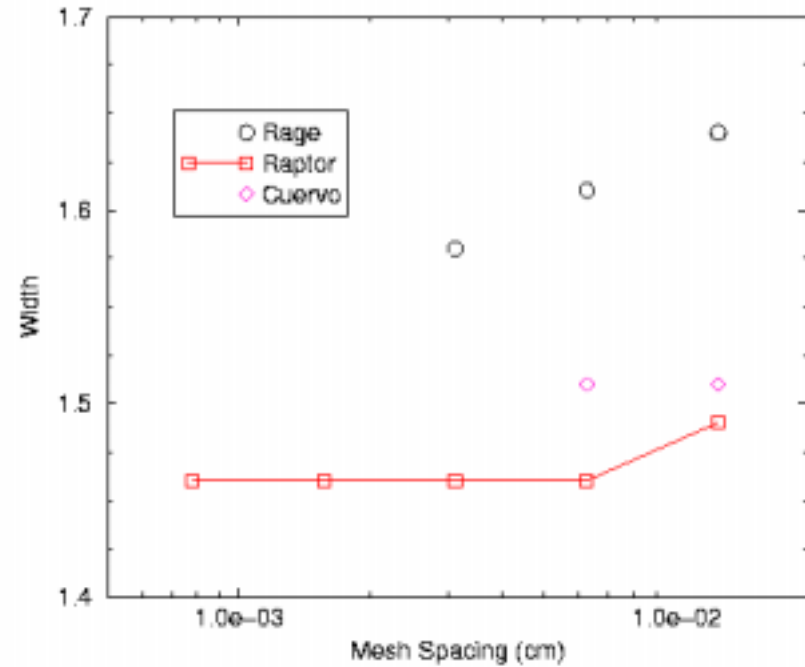
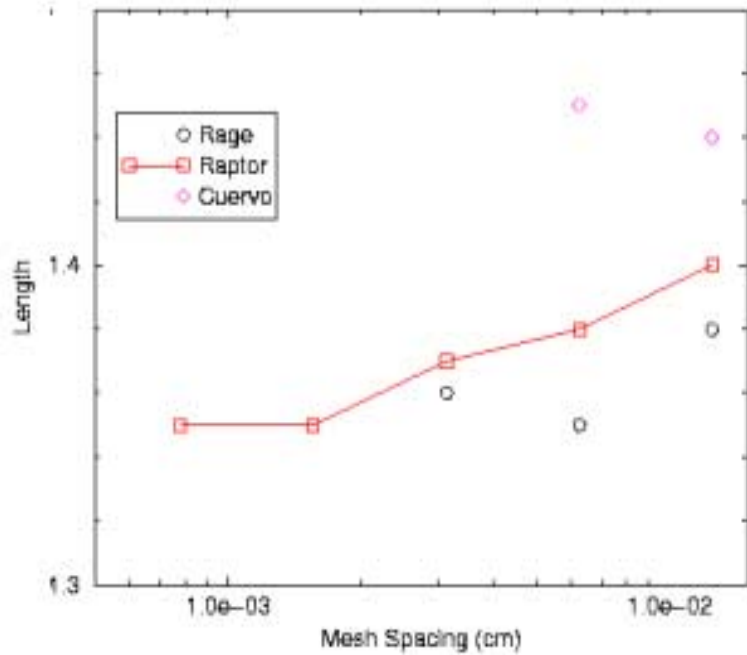


1.35cm

3.90625 micron zoning



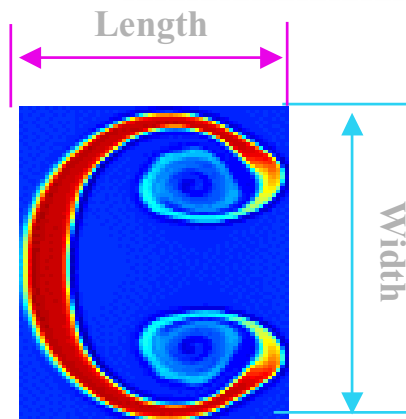
Integral Lengths - Summary



Convergence Rates

$$\text{Cuervo} \sim \Delta x^{1.28}$$

$$\text{Raptor} \sim \Delta x^{1.58}$$

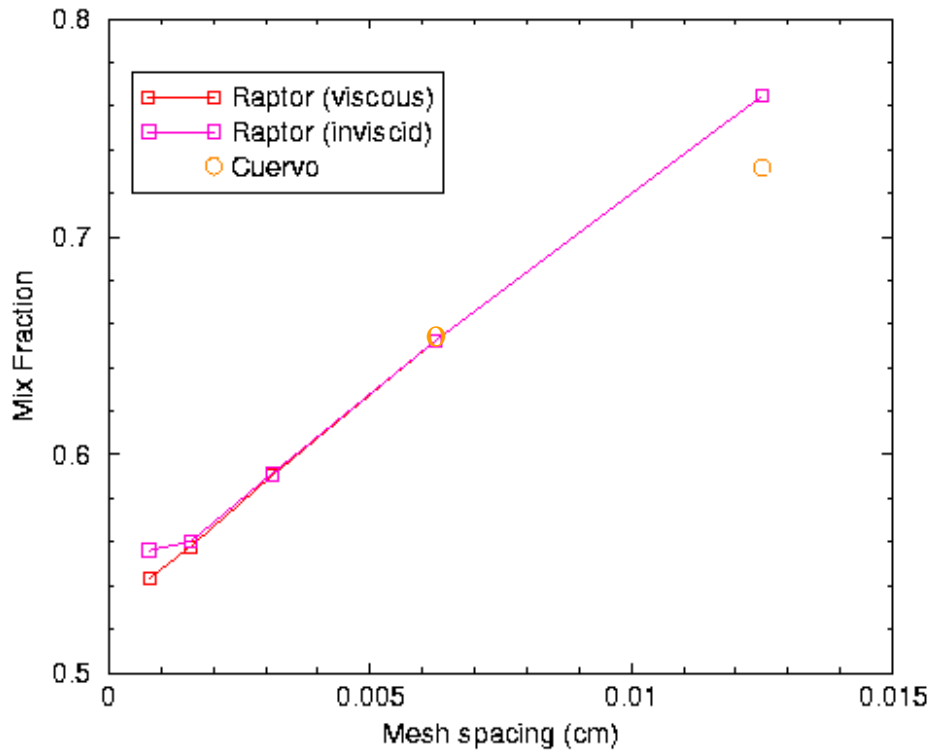


Convergence Rates

$$\text{Cuervo} \sim \Delta x^{0.74}$$

$$\text{Raptor} \sim \Delta x^{0.28}$$

Mixing Fraction



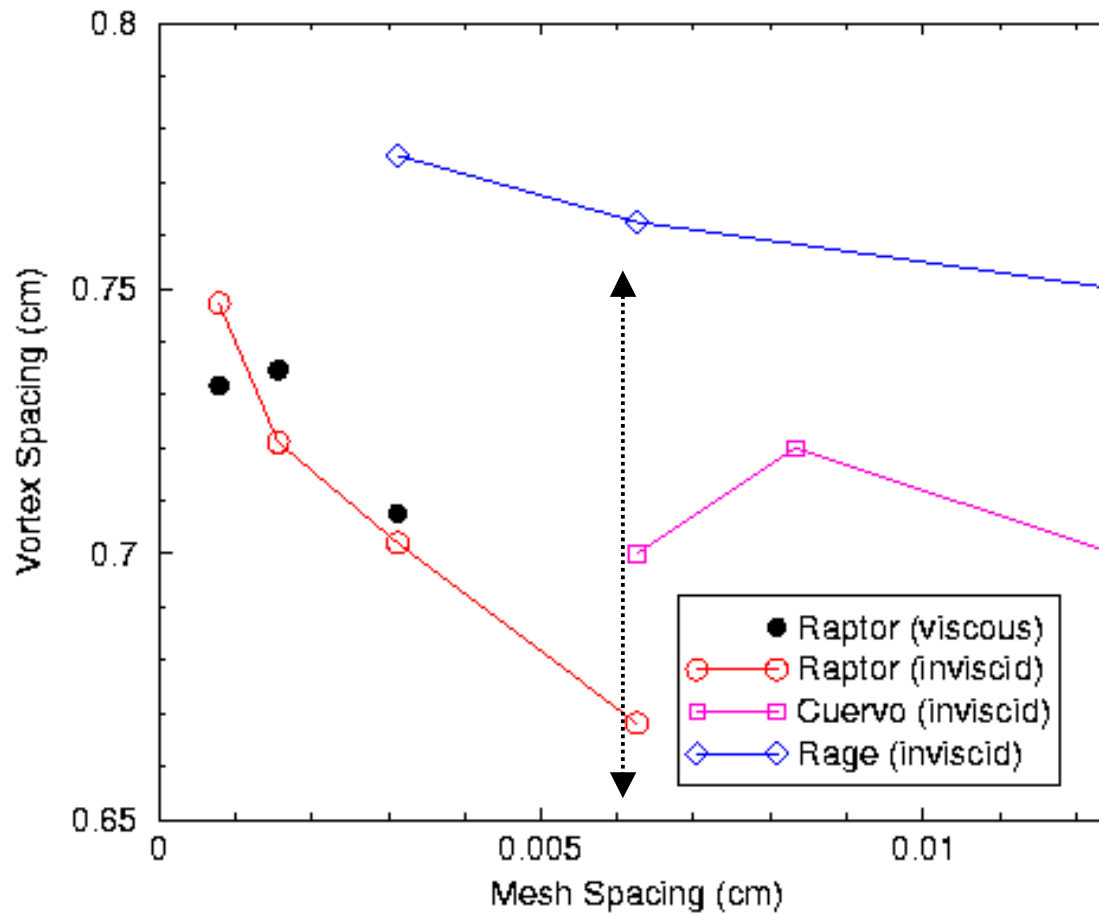
$$\theta = \frac{\sum f_{\text{SF}_6} (1-f_{\text{SF}_6}) \Delta x \Delta y}{(\sum f_{\text{SF}_6} \Delta x \Delta y) (\sum (1-f_{\text{SF}_6}) \Delta x \Delta y)}$$

Convergence Rates

$$\text{Cuervo} \sim \Delta x^{0.28}$$

$$\text{Raptor} \sim \Delta x^{1.02}$$

Vortex Spacing



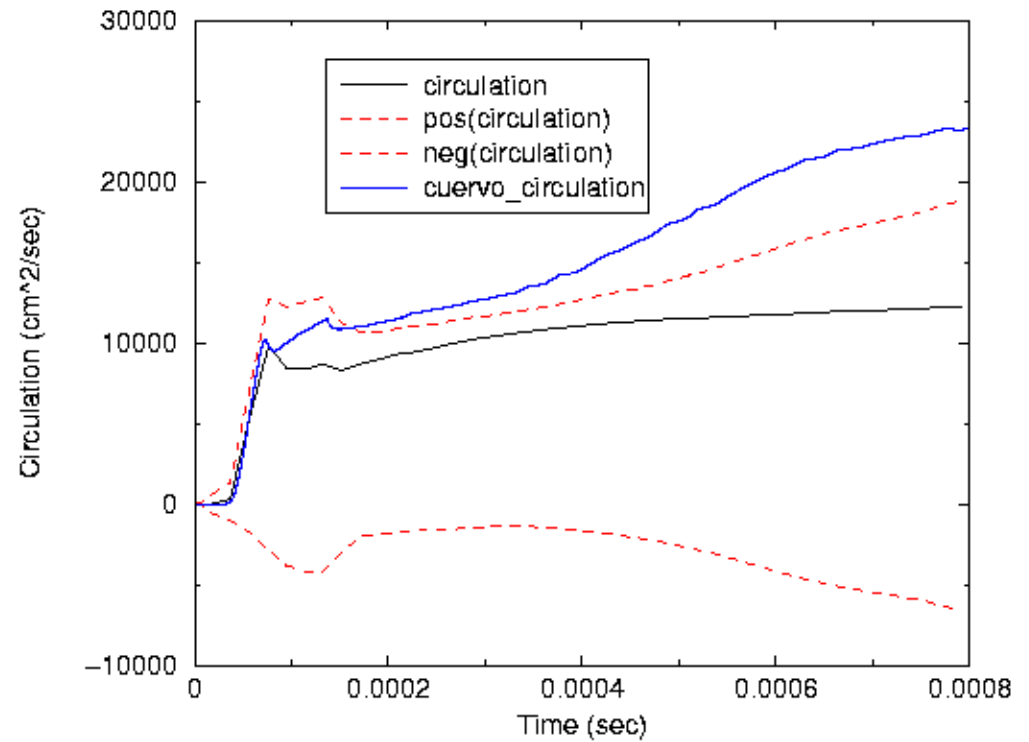
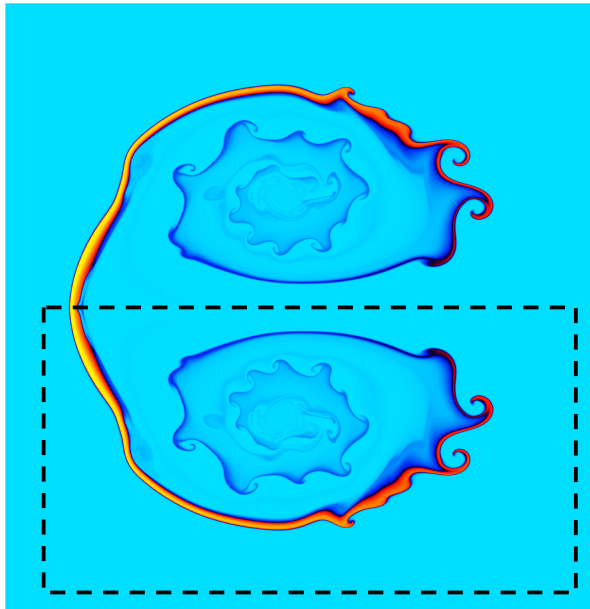
- Experimental data range shown for comparison

- cf. J.W. Jacobs, Phys. Fluids 1993; M=1.095, D=0.43

Convergence Rates

$$\text{Raptor} \sim \Delta x^{0.87}$$

Circulation Budget



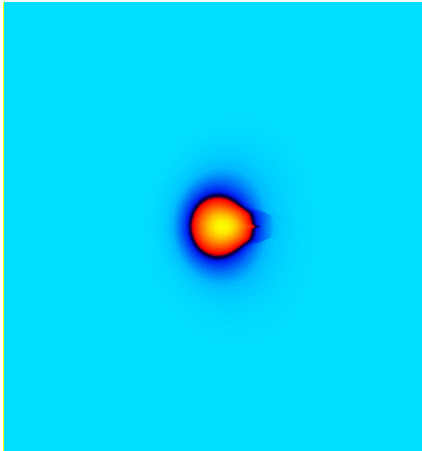
- Deposition by shock (positive)
- Counter-sign production (baroclinic)
- Late-time equilibration

Flow Dynamics

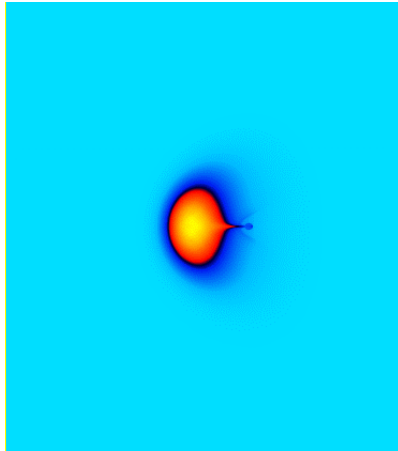
- Early time
 - Vortex blob deposition (shock-passage time $\sim 30 \mu\text{sec}$)
- Intermediate time
 - Blob dipole transformation
 - Counter-sign production
- Later time
 - Dipole configuration established
 - Balanced net vorticity (i.e. $\Gamma \sim \text{constant}$)

Flow Dynamics - Density

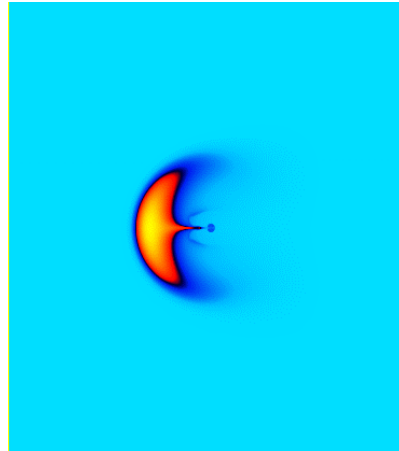
$t = .08\text{msec}$



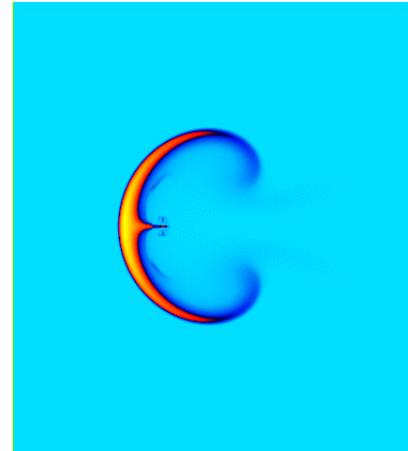
$t = .12\text{msec}$



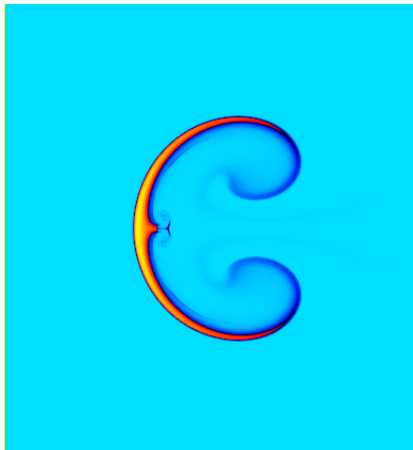
$t = .22\text{msec}$



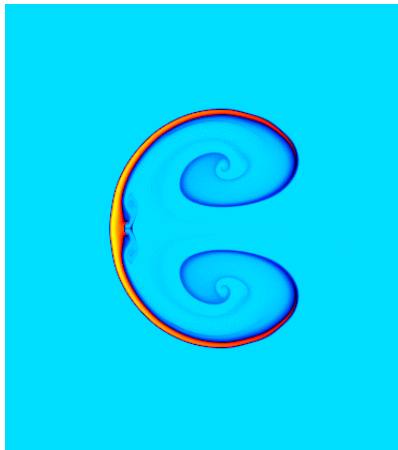
$t = .35\text{msec}$



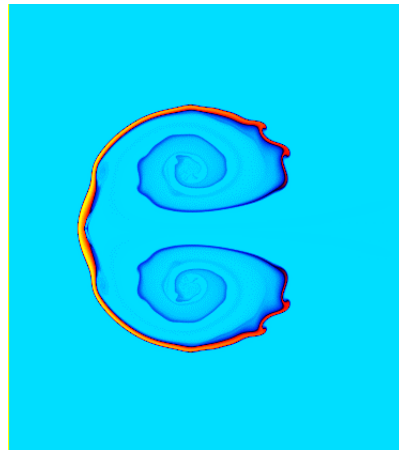
$t = .47\text{msec}$



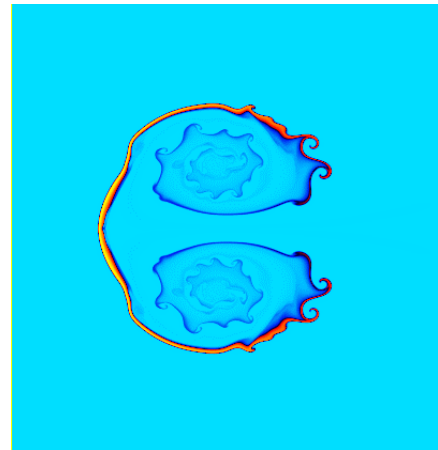
$t = .58\text{msec}$



$t = .70\text{msec}$

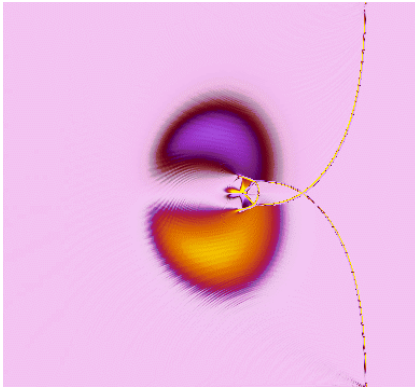


$t = .82\text{msec}$

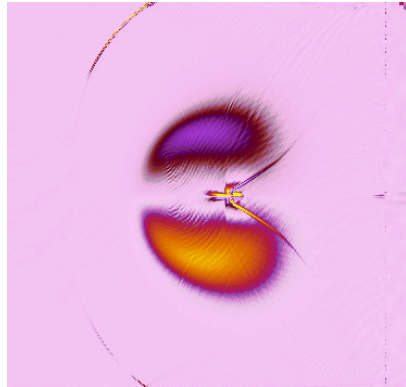


Flow Dynamics - Vorticity

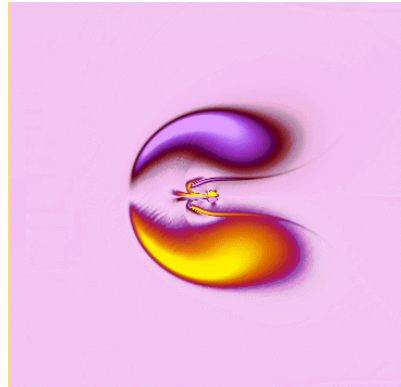
$t = .08\text{msec}$



$t = .12\text{msec}$



$t = .22\text{msec}$



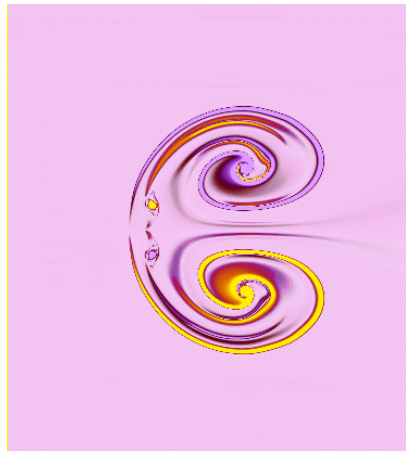
$t = .35\text{msec}$



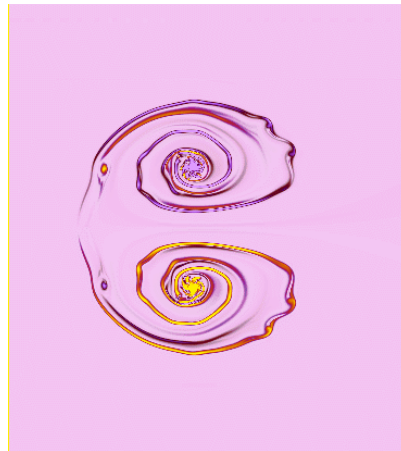
$t = .47\text{msec}$



$t = .58\text{msec}$



$t = .70\text{msec}$

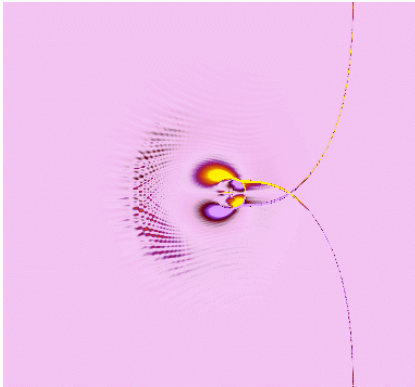


$t = .82\text{msec}$

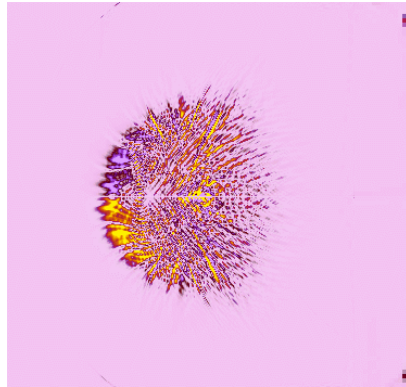


Flow Dynamics – Baroclinic Generation

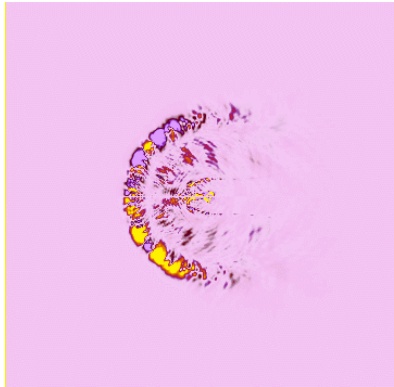
$t = .08\text{msec}$



$t = .12\text{msec}$



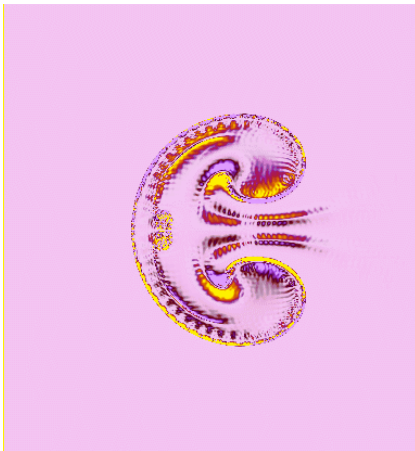
$t = .22\text{msec}$



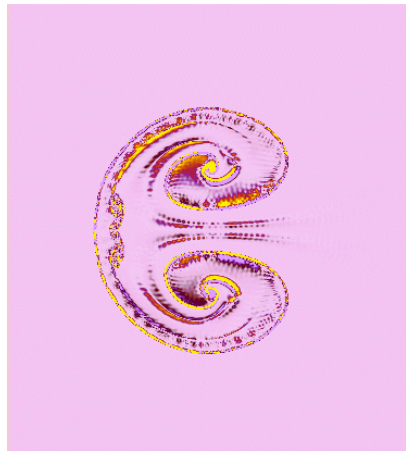
$t = .35\text{msec}$



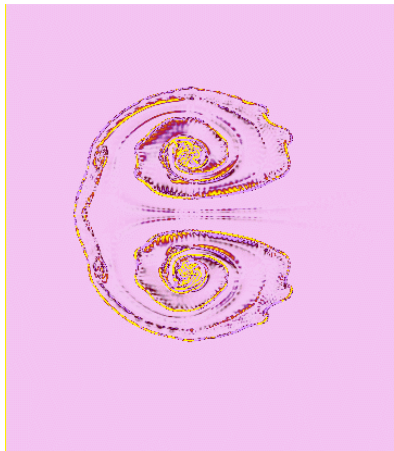
$t = .47\text{msec}$



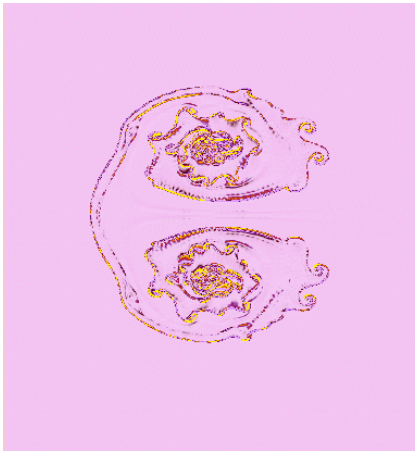
$t = .58\text{msec}$



$t = .70\text{msec}$

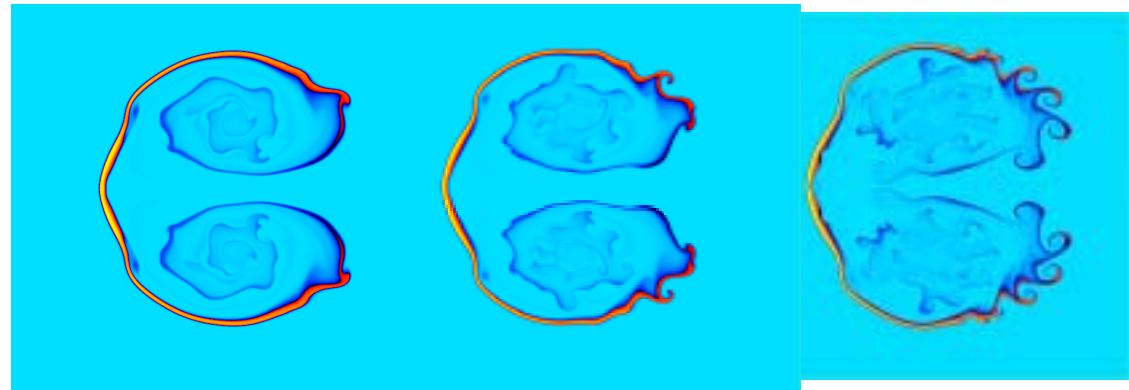


$t = .82\text{msec}$



Raptor Summary

31.25 μm , 15.625 μm , 7.8125 μm



Increasing Resolution

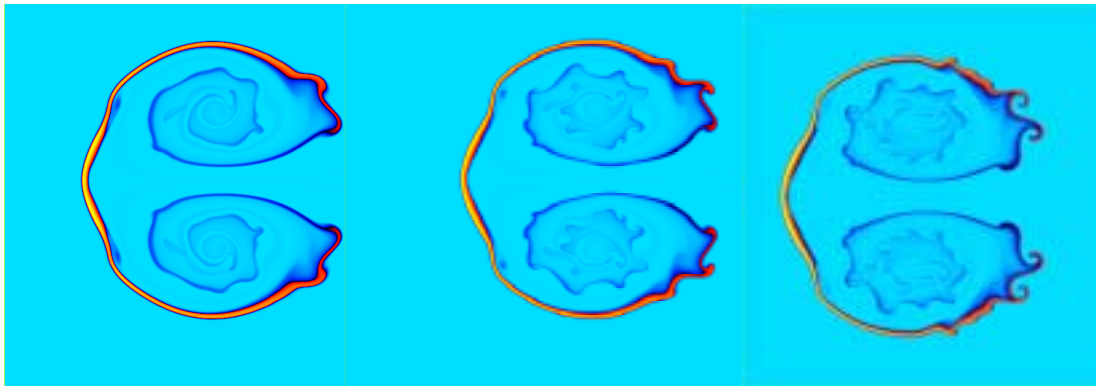


Inviscid

Increasing Resolution



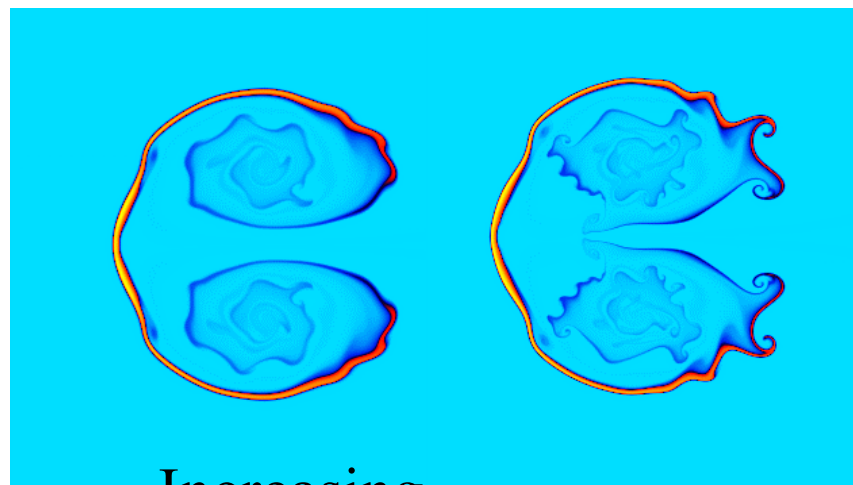
Viscous



NEW Raptor Summary

No prelat, viscosity fix

31.25 μm , 15.625 μm , 7.8125 μm



Increasing Resolution

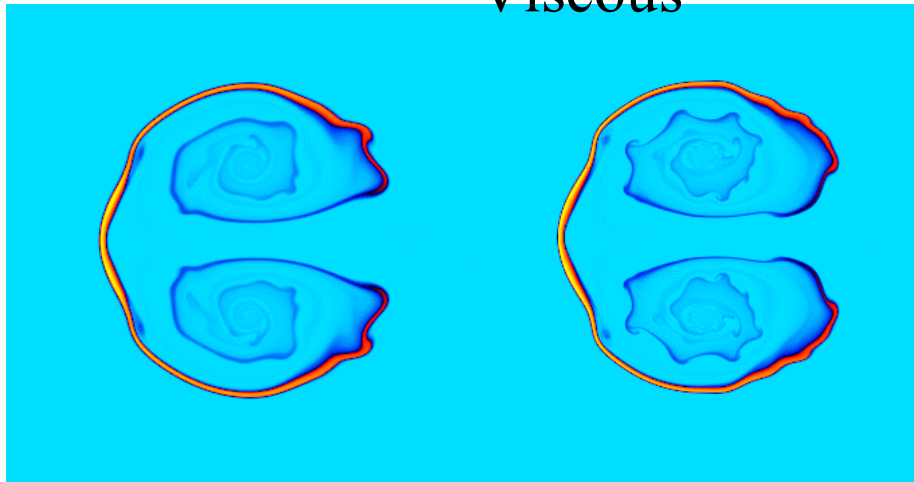


Inviscid

Increasing Resolution



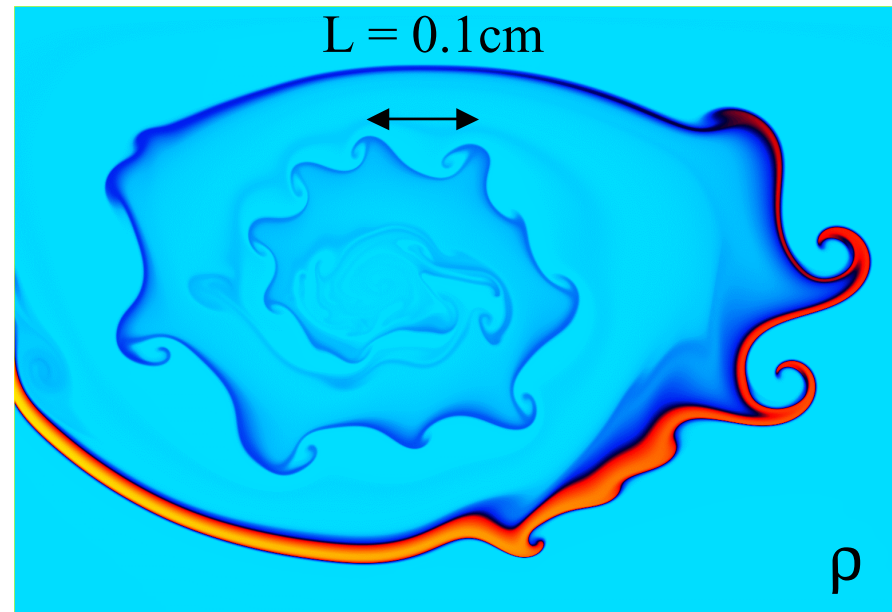
Viscous



Lengthscale estimates

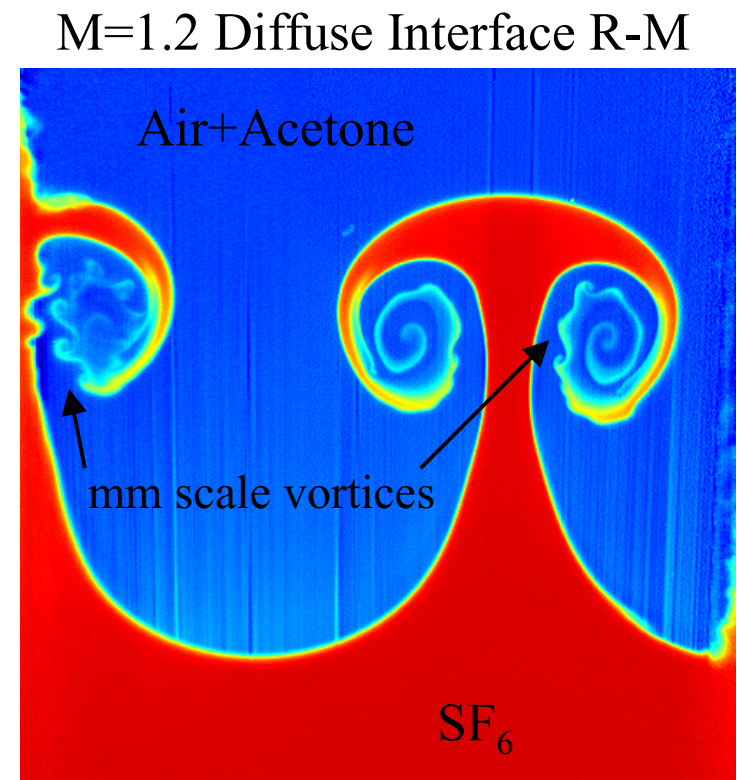
- Using order of magnitude considerations (Tennekes and Lumley)
 - $U \approx 2,000$ cm/sec, $\nu \approx 0.1$ cm²/sec, $L = 0.1$ cm $Re = 2,000$
 - $\eta/L \sim Re^{-0.75}$ $\eta \sim 3$ μ m (Kolmogorov scale)
 - $\lambda/L \sim Re^{-0.5}$ $\lambda \sim 90$ μ m (Taylor scale)

- At 7.8125 μ m resolution, we have about 12 points/ λ resolvable



Conclusions

- Have we demonstrated convergence?
 - Maybe. Some diagnostics show convergence while others do not.
 - Include additional diagnostics (statistical, wavelet analysis).
- Have demonstrated what resolutions and physics are required for resolved calculations.
- Directly compute mm wavelength vortices. This is a robust feature present in analogous flow (Jacobs' Diffuse Interface R-M).
- RAGE calculations appear to be the outlier; much more structure and different integral measurements. Vorticity?

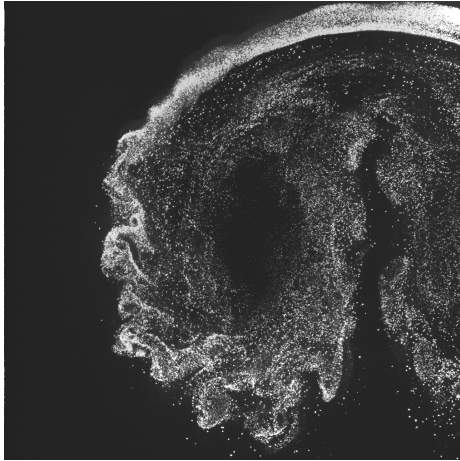


Courtesy of Prof. J.W. Jacobs

NEEDS

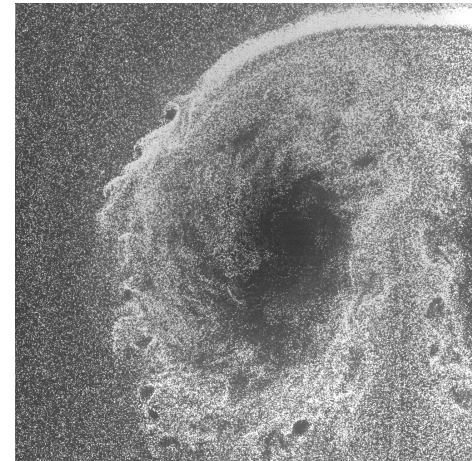
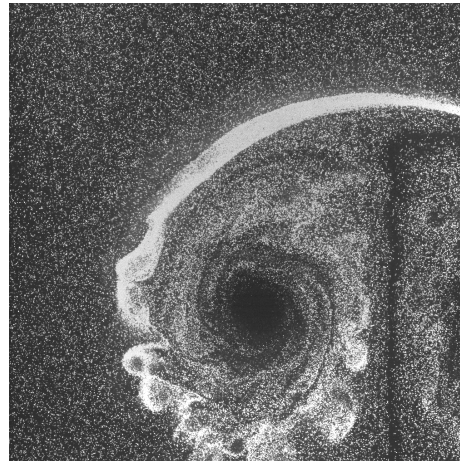
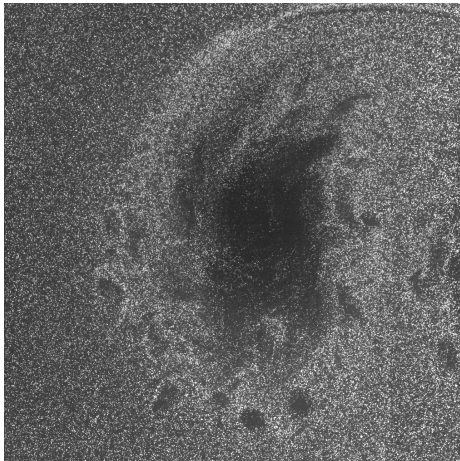
- High(er) resolution experimental imaging
 - PLIF visualization. LANL facility appears to generate a “more stable” evolving flow better pictures. Isolate mm-scale vortices
- More direct measurements
 - Mixing measurements (Rayleigh scattering). Complementary to Helium jet work by J. Budzinski.
- More computing resources (never have enough) would allow definitive simulations.
 - e.g. highest resolution run took ~ 70 hrs wall clock on 128 CPU's of an SP-3; AMR required 4.7 Mzones compared to 43 Mzones single grid.

LANL Experimental Activity



- No outer flow seeding

Varying the seeding densities & light intensity



Images courtesy C. Tomkins, LANL, DX-3